

Basilisk (Gerris) Users' Meeting 2025



Simulation of melting/icing problems with the phase-field method

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Research Background and Present Scenario

Limitations of Phase Field Models and Improvements

Verification Cases

- Stefan Problem
- Rayleigh-Bénard Convection
- Ice Growth on Cylinder in Flow
- Vertical Convection

Conclusion & Outlook



Research Background

Melting and icing phenomena are common in nature and human life.







Smedsrud, L. H. *et al.* (2022) *Rev. Geophys.*

Atlantic inflow cooling and sea ice variation Cenedese, C. *et al.* (2023) *Annu. Rev. Fluid Mech.*

> Iceberg Melting

Icing on aircraft wings



Phase-field methods have been widely adopted for studying melting and icing problems.



Weady, S. *et al.* (2022) *Phys. Rev. Lett.*



Yang, R. *et al.* (2023) J. Fluid Mech.



ice front $\phi = 0.5$



Phase-field methods can yield non-physical results.

Advantages:

- Easy topological change handling
- Exact energy conservation
- Easy multiphase extension

Disadvantages:

Non-physical motion of the ice front

- High local curvature
- Low Stefan number



Traditional phase-field methods have difficulty with accurate temperature boundary conditions at the ice front.

Navier-Stokes Equations $\rho\left(\frac{\partial u}{\partial t} + u \cdot \nabla u\right) = -\nabla P + \frac{1}{Re}\nabla^2 u - \frac{\rho}{Fr}e_g + f_p$ $\nabla \cdot u = 0$

Energy Equation

 $\frac{\partial \theta}{\partial t} + \nabla \cdot (\boldsymbol{u}\theta) = \frac{1}{\rho C_p} \nabla [k_{\mathrm{T}} \nabla \theta] - St \frac{\lambda_{\rho}}{\rho C_p} \frac{\partial \phi}{\partial t}$

Phase-Field Model (Allen-Cahn Equation)

$$\frac{\partial \phi}{\partial t} = M \left[\nabla^2 \phi - \frac{1}{4\epsilon^2} \frac{dg}{d\phi} \right] + \frac{M}{\epsilon^2} \frac{df}{d\phi} (\theta - \theta_m)$$

$$\mathbf{I}$$
at the ice front: $\theta_{\Gamma} \neq \theta_m$



Challenges faced by traditional phase field methods



- Small-scale structures are smoothed
- Ice and water cannot coexist at melting point



Original Phase-Field Model:

$$\frac{\partial \phi}{\partial t} = M \left[\nabla^2 \phi - \frac{1}{4\epsilon^2} \frac{dg}{d\phi} \right] + \frac{M}{\epsilon^2} \frac{df}{d\phi} (\theta - \theta_m)$$

Improved Phase-Field Model:

$$\frac{\partial \phi}{\partial t} = M \nabla^2 \phi - M \nabla \cdot \left[\frac{\phi(1-\phi)}{\sqrt{2}\varepsilon} \mathbf{n} \right] + \frac{M}{\varepsilon^2} \phi (1-\phi) \left(\theta - \theta_m^{eff} \right)$$

Remove curvature effect

Introduce effective melting point θ_m^{eff}

• At the ice front:

$$\theta_{\Gamma} - \theta_m = 0$$

- Maintain the original equilibrium form and stability: $\phi = \frac{1}{2} \left[1 + \tanh\left(\frac{x}{2\sqrt{2}\varepsilon}\right) \right]$
- Energy conservation.



- > Initialization: Set $\theta_m^{eff,0} = \theta_m$
- > Prediction step :
- Advance ϕ^n using $\theta_m^{eff,n}$ to obtain ϕ^* ;
- Compute the temperature at the ice front and use its deviation from the melting point to update the effective melting point.

$$\theta_{\Gamma} = \theta_{i,j} + l \nabla \theta_{i,j} \cdot \boldsymbol{n}_{i,j}$$
$$\theta_{m}^{eff,n+1} = \theta_{m}^{eff,n} - (\theta_{\Gamma} - \theta_{m})$$



Correction step:

• Advance ϕ^{n+1} using the updated effective melting point $\theta_m^{eff,n+1}$



The improved phase-field model accurately captures small-scale structures.

Melting of an icicle



Uniform initial temperature: $\theta = \theta_m$



 Improved Phase-Field Model Original Phase-Field Model



Improved phase-field model removes curvature effects and ensures ice-water coexistence.

> Ice–Water Coexistence Validation



• Ice circle radius evolution

Uniform initial temperature: $\theta = \theta_m$



• Ice circle radius change ratio



Good agreement with previous results





12

• Average water height at steady state



Adaptive mesh refinement near the ice front



Inflow temperature $T_{\infty} = 2.5^{\circ}C$

Cooled pipe temperature -7.5° C Inflow velocity V_{∞} = 0.01m/s



Ice front profile comparison



Suitable for **3D** simulations





- ➢ An improved phase-field model is proposed to eliminate curvature-induced artifacts and introduce an effective melting point, ensuring that the temperature at the ice front equals the melting point.
- The improved model demonstrates superior performance in both classical Stefan problems and complex flow simulations.
- \succ The code will be released soon on Sandbox.

"The development of an improved phase-field method for simulating freezing/melting problems in turbulent environments" to be submitted to the *J. Comput. Phys.*



Outlook

Future Work: ice-water phase transition in the presence of air

> Droplet freezing



	ho [kg/m ³]	μ [Pa·s]	$\alpha \ [m^2/s]$	$C_p [J/(kg^{\circ}C)]$
Air	1.29	1.70×10^{-5}	2.00×10^{-5}	1.00×10 ³
Water	1.00×10^{3}	1.70×10^{-3}	1.32×10^{-7}	4.21×10^{3}
Ice	9.17×10^{2}	1.70×10^{-3}	1.18×10^{-6}	2.03×10^{3}



• Ice front profile comparison



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Thank You for Your Attention

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