

Implementation of a $k - \epsilon$ RANS turbulence model in Basilisk

Basilisk Gerris User Meeting 2025

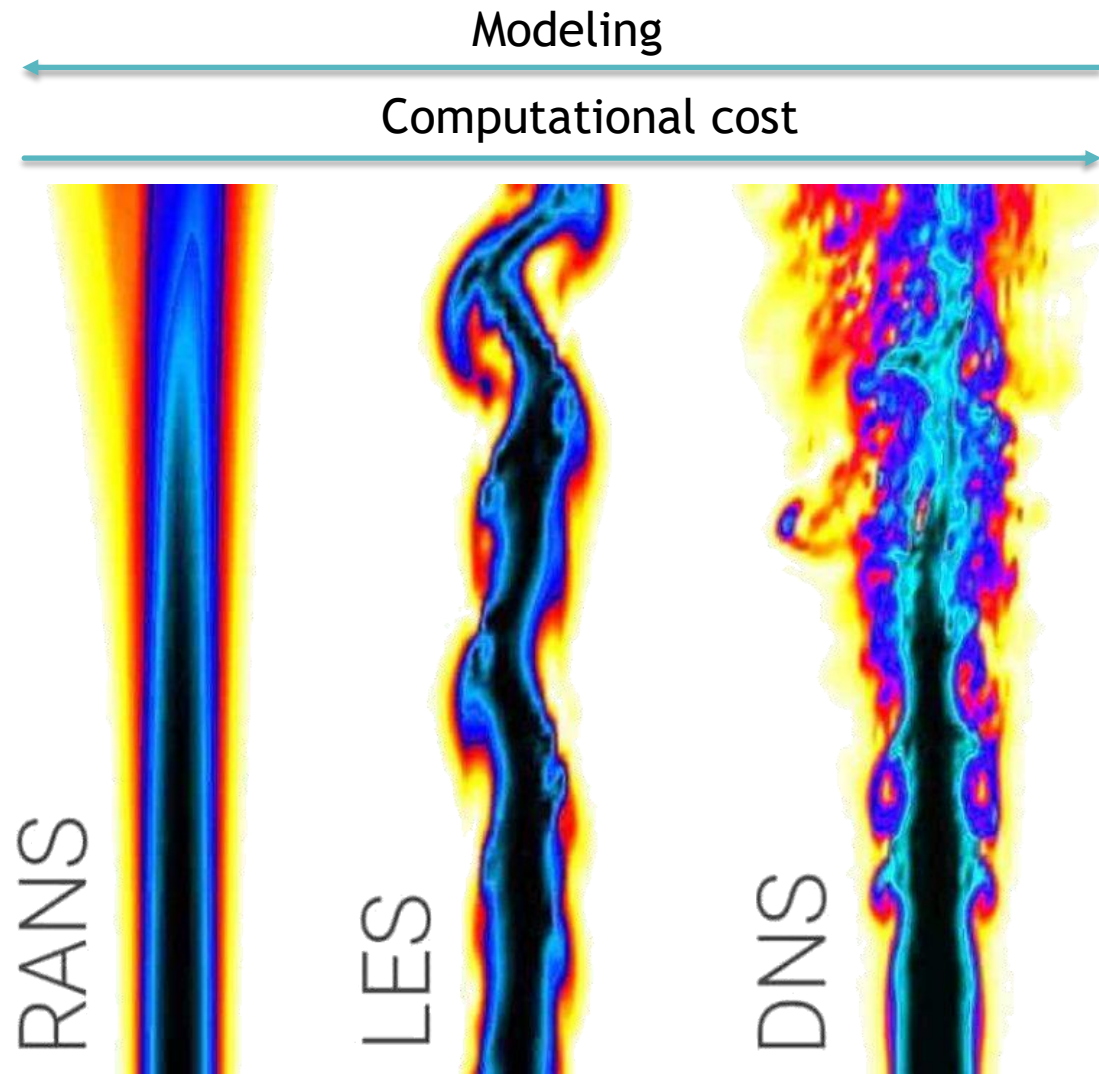


Turbulence



<https://gauss.math.yale.edu>

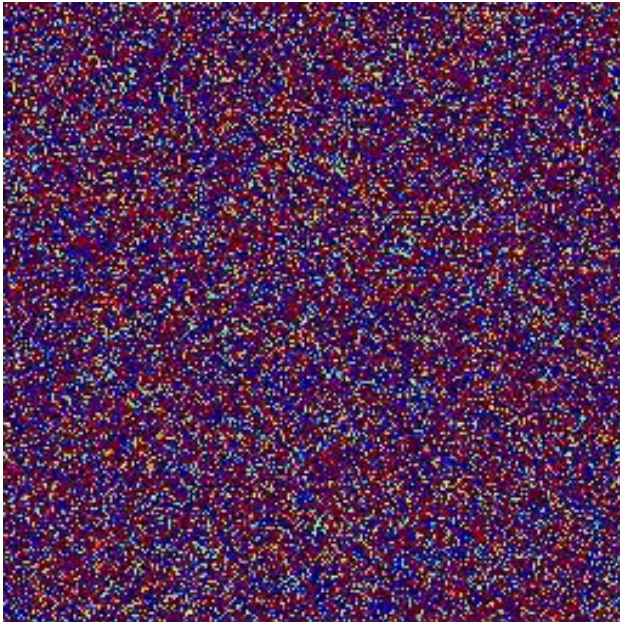
Computation of Turbulence



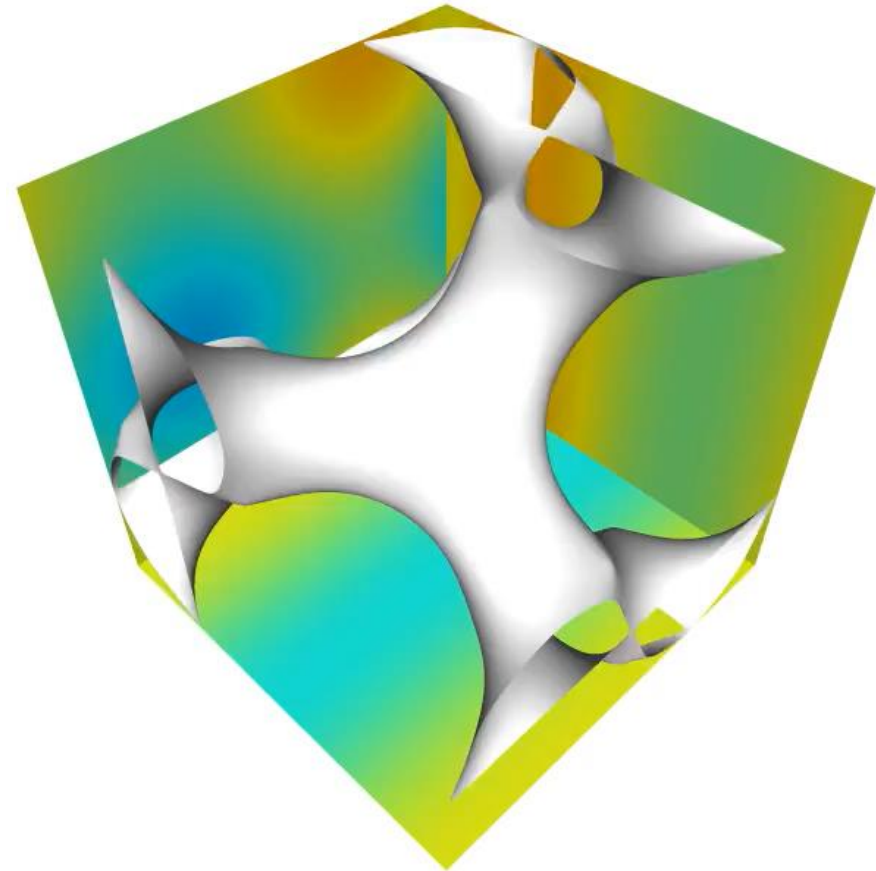
- ▶ DNS (Direct Numerical Simulation) : no model
- ▶ LES (Large Eddy Simulation) : small scales modeled
- ▶ RANS (Reynolds Average Navier-Stokes) : Average of the flow
 - ▶ Mostly used by industry

Turbulence in Basilisk

- ▶ Mostly DNS :
 - ▶ Isotropic turbulence



Examples/turbulence.c in 2D



Examples/isotropic.c in 3D

- ▶ Some case of modeling in sandboxes : Antoon van Hooft (LES)

RANS model

- Average of the Navier Stokes equation

$\phi = \bar{\phi} + \phi' : \bar{\phi}$ mean part, ϕ' fluctuation

$$\rho \left(\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial \bar{u}_i \bar{u}_j}{\partial x_j} \right) = - \frac{\partial \bar{p}}{\partial x_i} + \frac{\partial}{\partial x_j} \left(\mu \frac{\partial \bar{u}_i}{\partial x_j} \right) - \frac{\partial}{\partial x_j} \underbrace{(\rho \overline{u'_j u'_i})}_{\text{Reynolds tensor}}$$

Boussinesq hypothesis : $\overline{\rho u'_j u'_i} = \mu_t S_{ij} \quad S_{ij} = \frac{1}{2} \left(\frac{\partial \bar{u}_i}{\partial x_j} + \frac{\partial \bar{u}_j}{\partial x_i} \right)$

- $k - \epsilon$ model

Dimensional analysis : $\mu_t \propto \rho \frac{k^2}{\epsilon}$

$k = \frac{1}{2} \overline{u'_i u'_i}$ turbulent kinetic energy

$\epsilon = \nu \overline{\frac{\partial u'_i}{\partial x_j} \frac{\partial u'_i}{\partial x_j}}$ rate of dissipation

Turbulence modeling

- Equation for the $k - \epsilon$ [1]

— advection
— diffusion
— production
— dissipation

$$\mu_t = \rho C_\mu \frac{k^2}{\epsilon}$$
$$\frac{\partial \rho k}{\partial t} + \frac{\partial \rho k u_i}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right] + P_k - \rho \epsilon$$

$$\frac{\partial \rho \epsilon}{\partial t} + \frac{\partial \rho \epsilon u_i}{\partial x_i} = \frac{\partial}{\partial x_j} \left[\left(\mu + \frac{\mu_t}{\sigma_\epsilon} \right) \frac{\partial \epsilon}{\partial x_j} \right] + C_{1\epsilon} \frac{\epsilon}{k} P_k - C_{2\epsilon} \rho \frac{\epsilon^2}{k}$$

$P_k = \mu_t S^2$ with S the norm of the deformation tensor

$$C_{1\epsilon} = 1.44, C_{2\epsilon} = 1.92, C_\mu = 0.09, \sigma_k = 1, \sigma_\epsilon = 1.3$$

Test on a 2D Mixing Layer

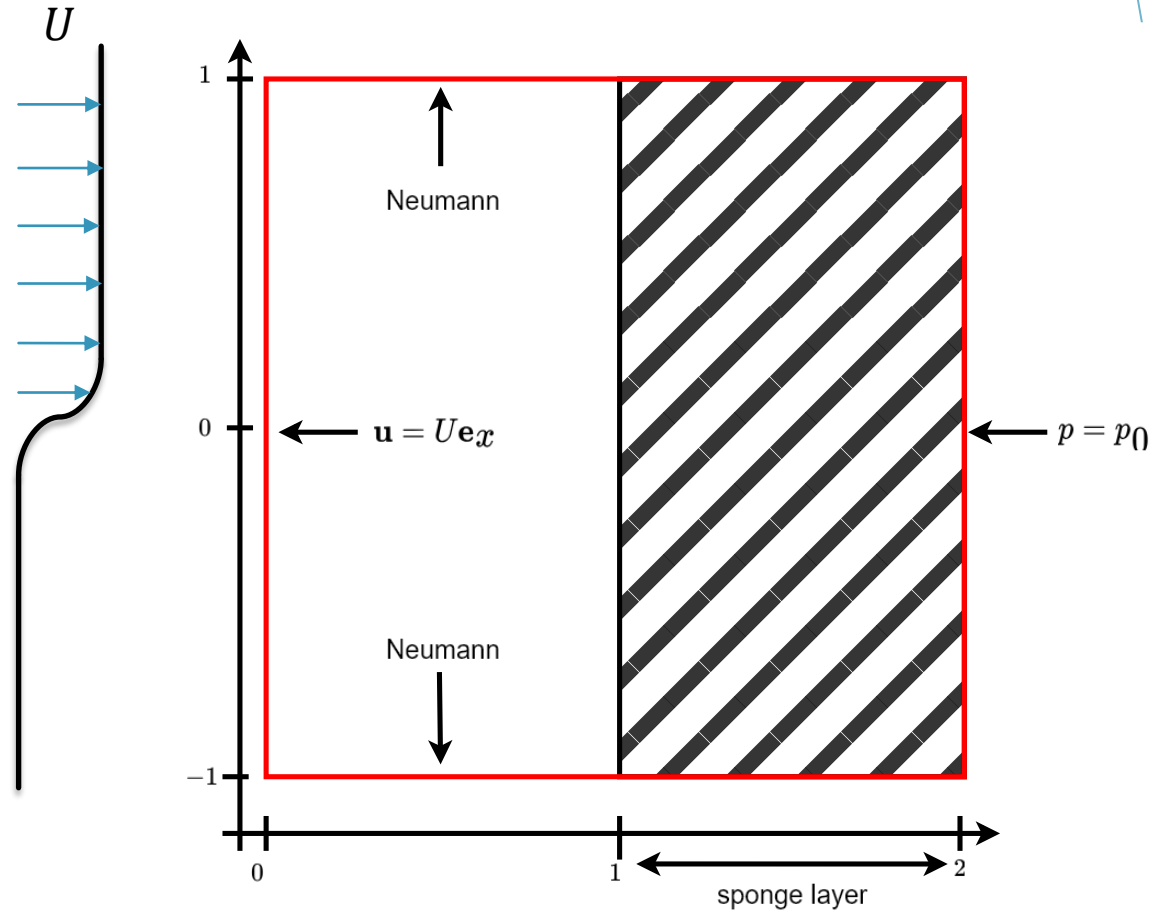
Upstream velocity:

$$U = U_1 \left(\frac{1}{2} + \frac{1}{2} \tanh \left(\frac{y}{\delta_i} \right) \right)$$

$$U_1 = 18 \text{ m.s}^{-1} [1]$$

$$\delta_i = 0.1 \text{ m}$$

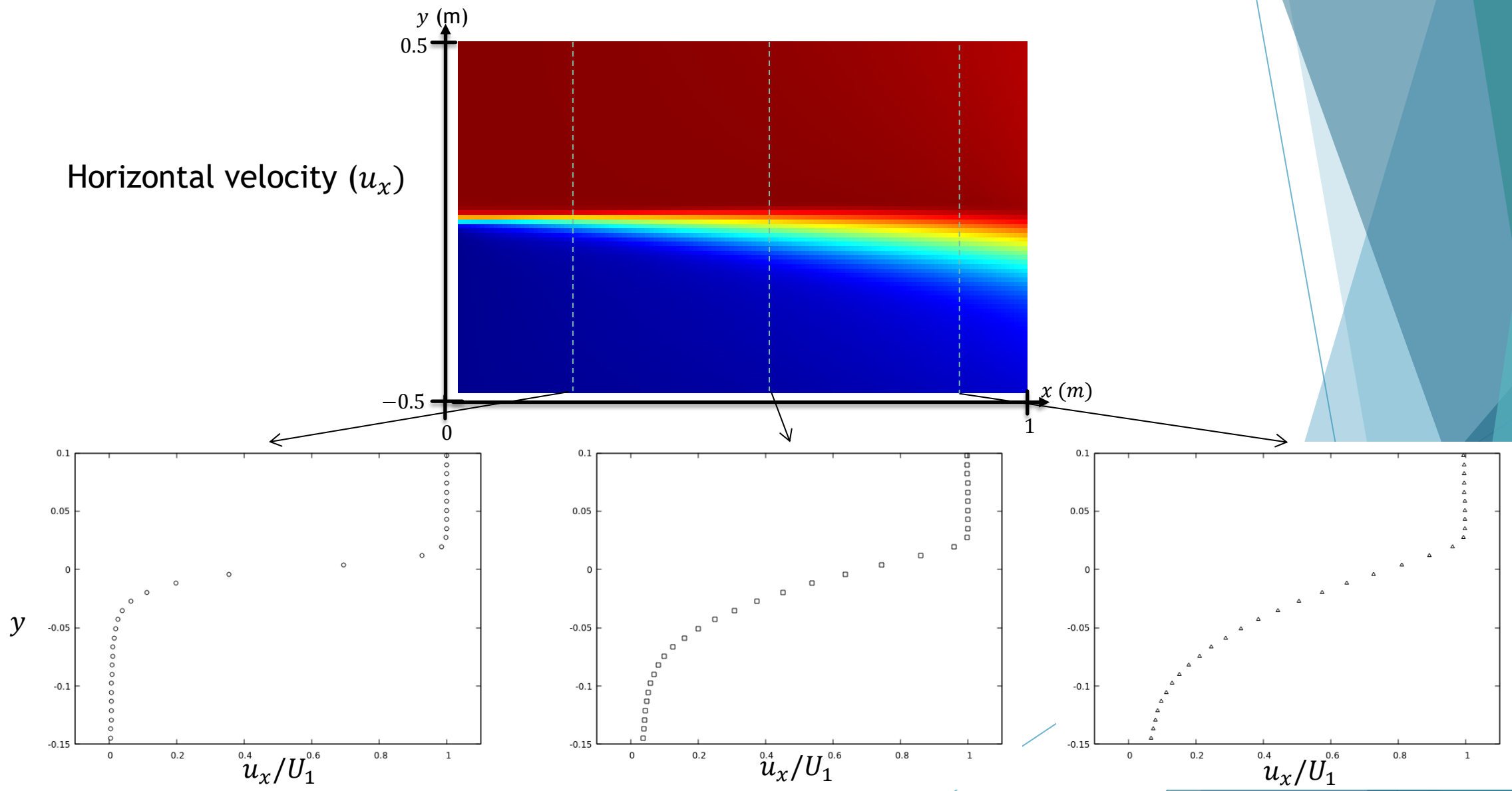
$$Re = \frac{\rho U_1 1}{\mu} = 2.34 \times 10^6$$



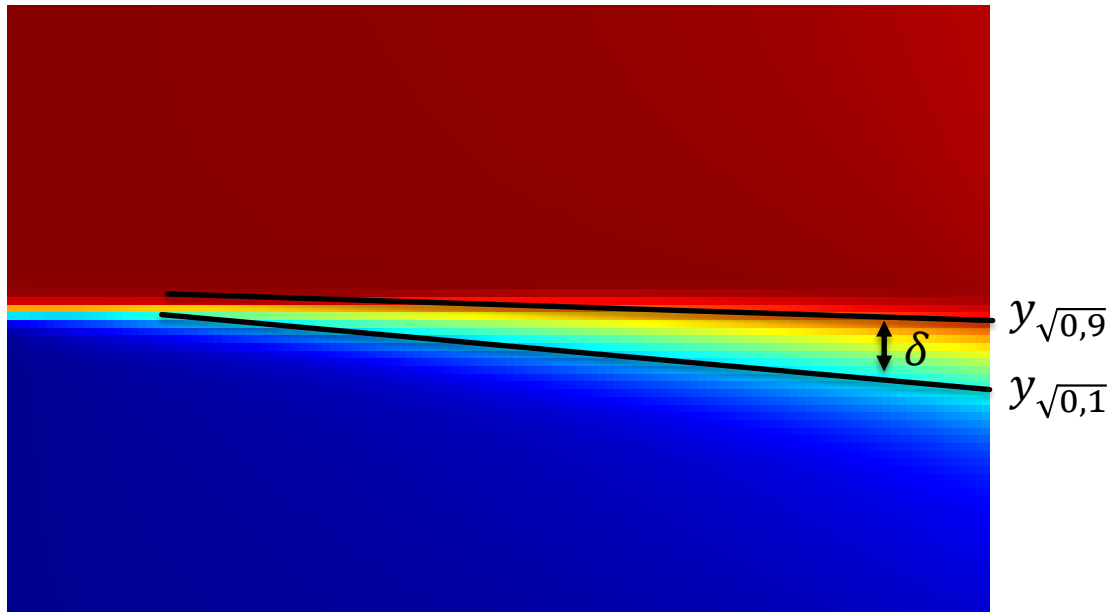
[1] Investigations of free turbulent mixing, H. W. Liepmann and J. Laufer, 1947

[2] Turbulence Modeling Validation, Testing, and Development, J. E. Bardina, P. G. Huang, T. J. Coakley, 1997

2D Mixing Layer : Results

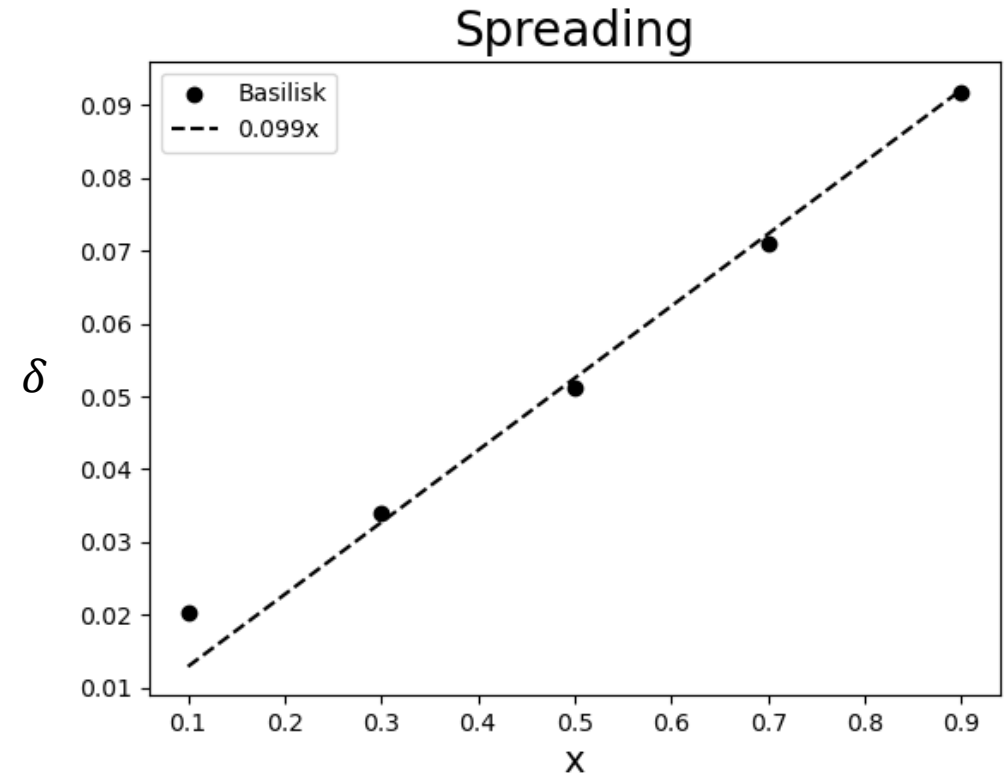


2D Mixing layer : Spreading



$$u_x(y_\alpha) = \alpha U_1$$

$$\text{Spreading : } \delta = y_{\sqrt{0,9}} - y_{\sqrt{0,1}}$$



Model	Spreading Rate
Experiment	0.115 $\pm$ 0.015
Launder-Sharma $k - \epsilon$ [1]	0.099
Basilisk	0.099

Boundary Layer close to a Solid

y^+ , u^+ inner non-dimensional variable

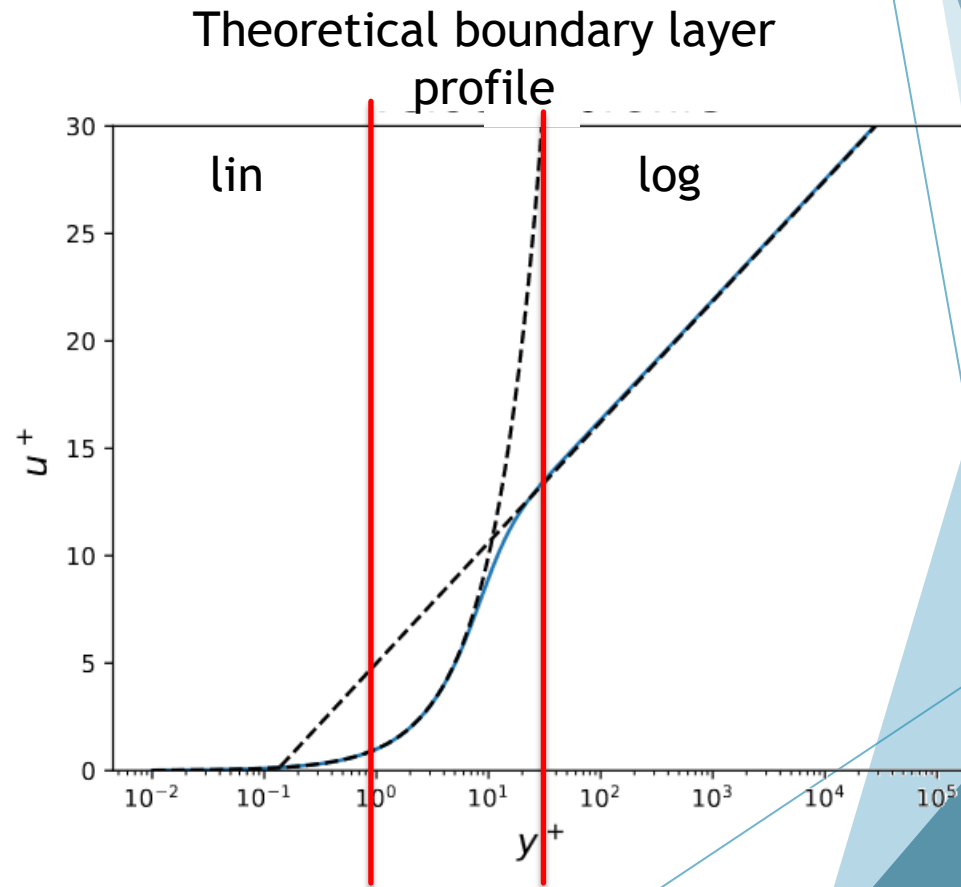
y^+ : vertical position

u^+ : tangential velocity

2 kinds of model depending on where is the first point above the wall

$y^+ > 30$: zone log $\rightarrow$ High Reynolds model

$y^+ < 1$: zone lin $\rightarrow$ Low Reynolds model



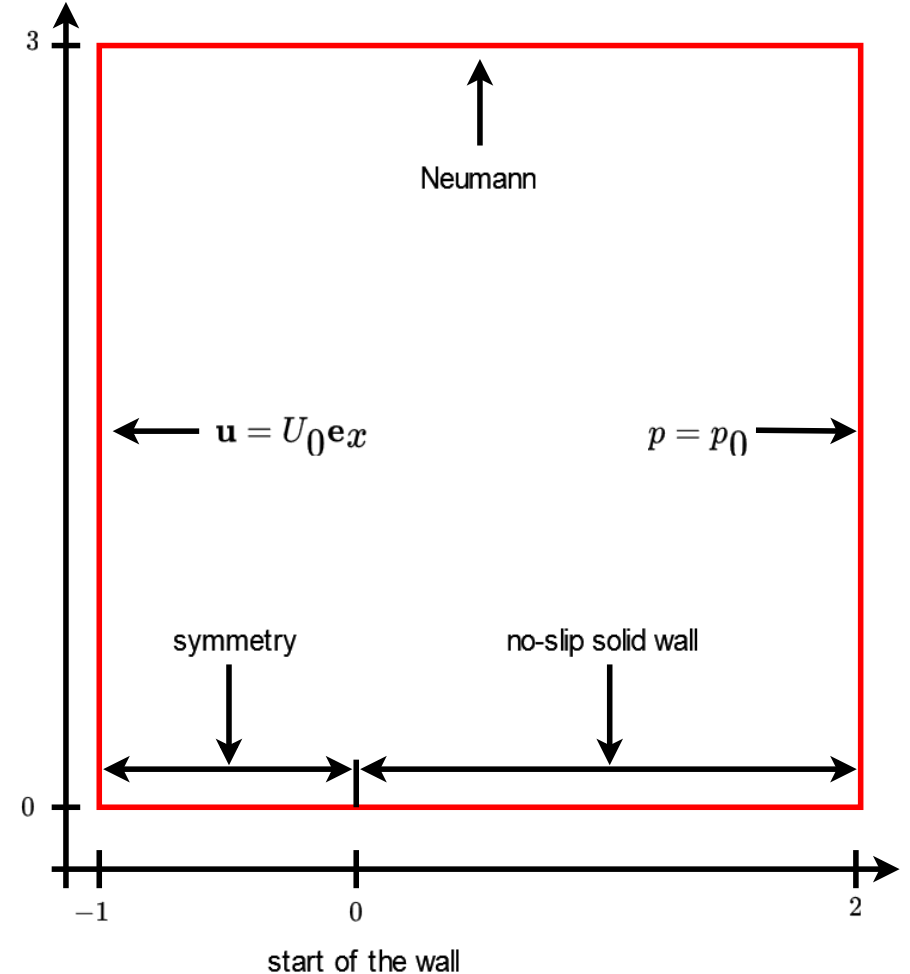
Basilisk classical solver uses isotropic mesh : use of high Reynolds model because $y^+ > 30$

Test on a 2D Flat Plate

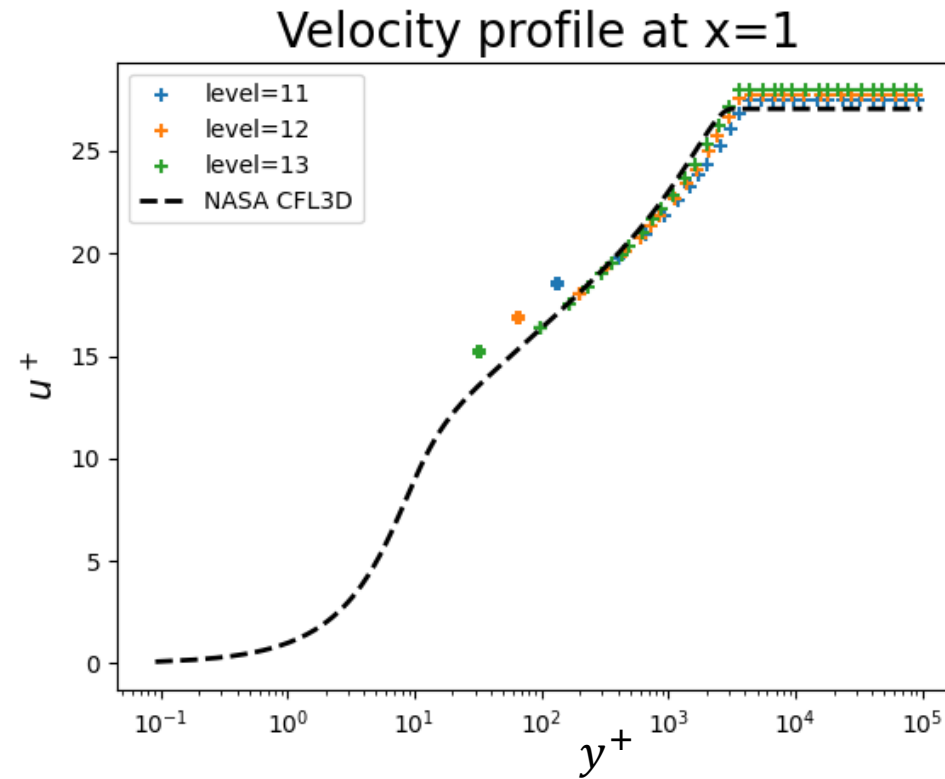
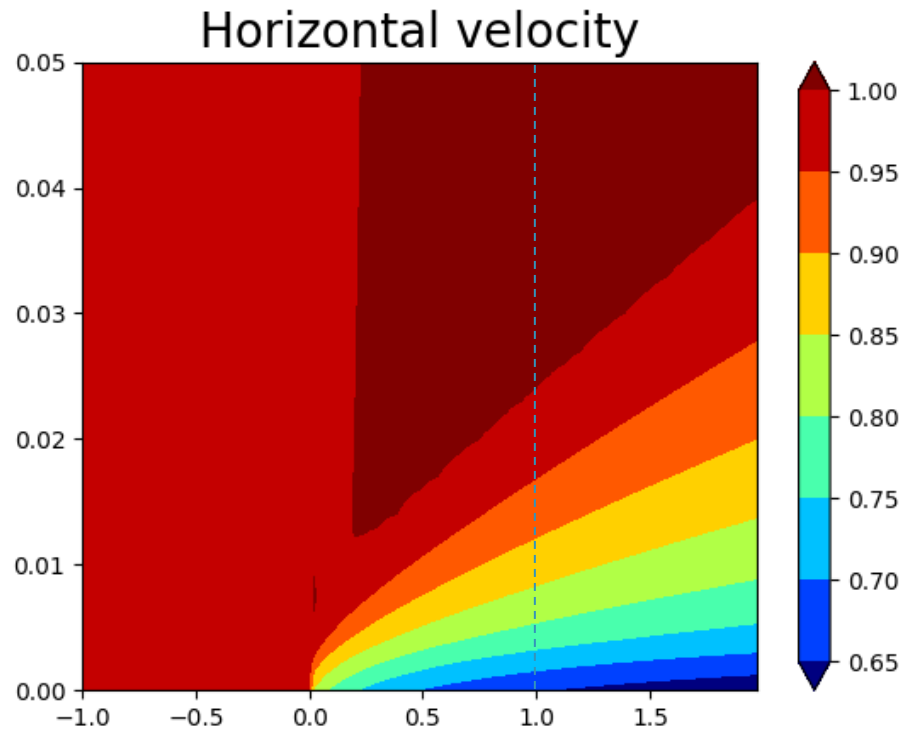
Examples from the Turbulence Modeling Resource of the NASA

Maxlevel	Minlevel	y^+ at $x = 1$	Number of cells
11	5	271	~16000
12	5	135	~60000
13	5	68	~132000

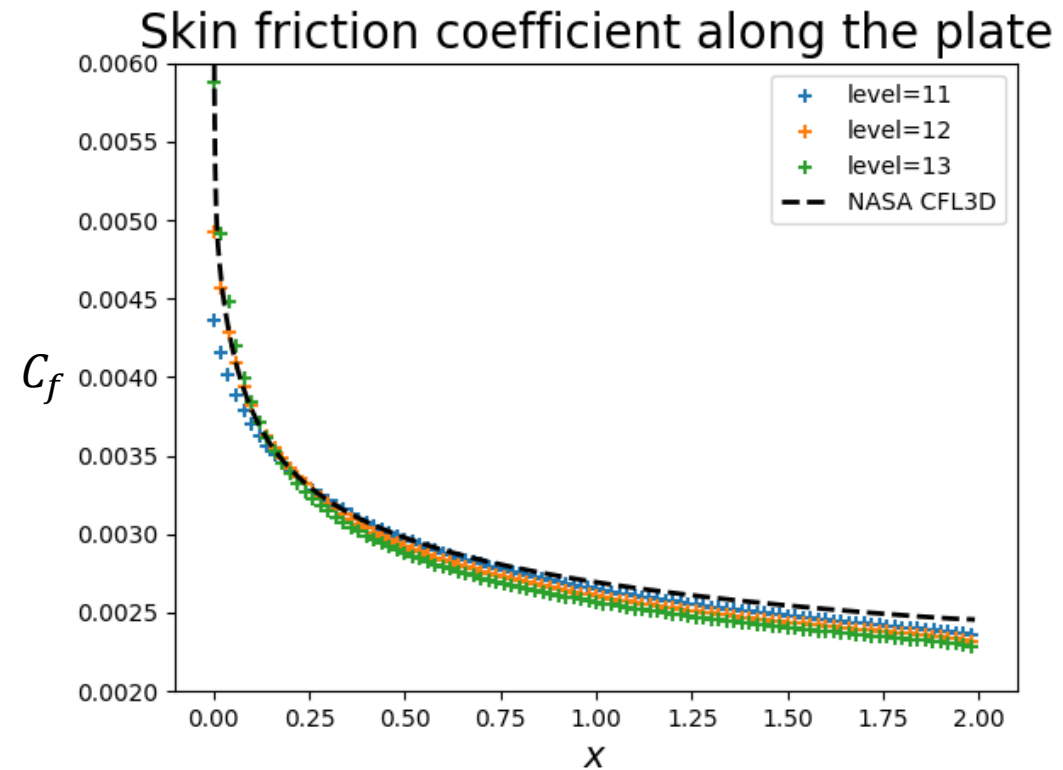
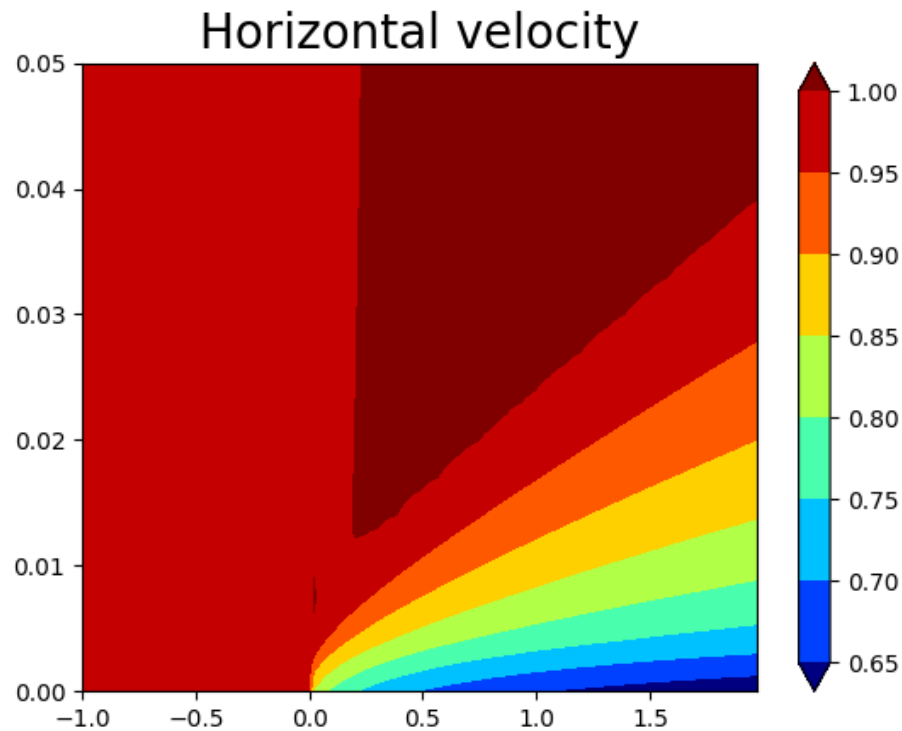
$$Re = \frac{\rho U_0 1}{\mu} = 5 \times 10^6$$



2D Flat Plate with High Reynolds Model



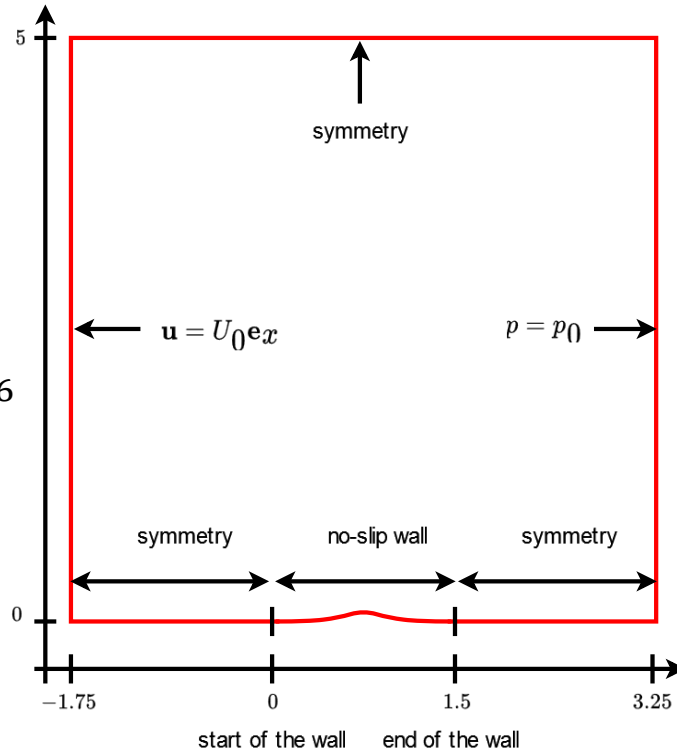
2D Flat Plate with High Reynolds model



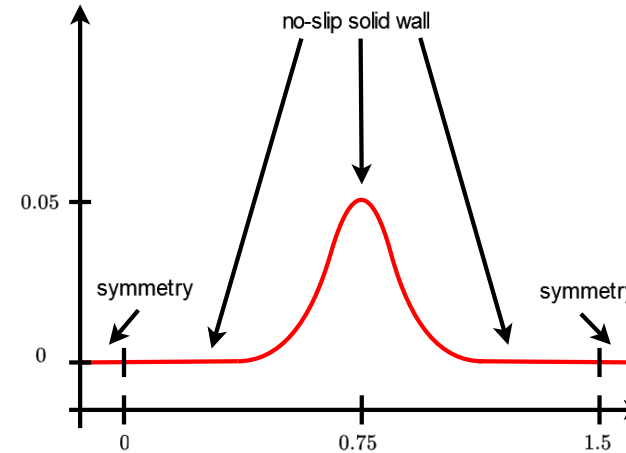
$$C_f = \frac{\mu \frac{\partial u_t}{\partial y}}{\frac{1}{2} \rho U_0^2}$$

2D Bump in a channel

$$Re = \frac{\rho U_0 1}{\mu} = 3 \times 10^6$$

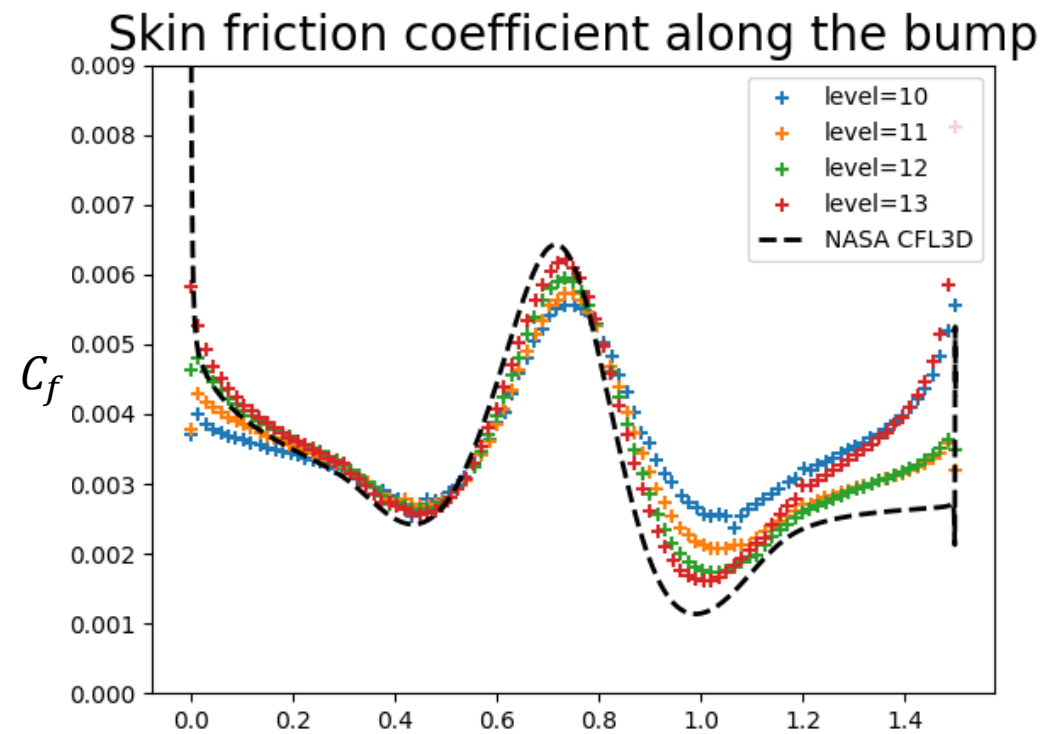
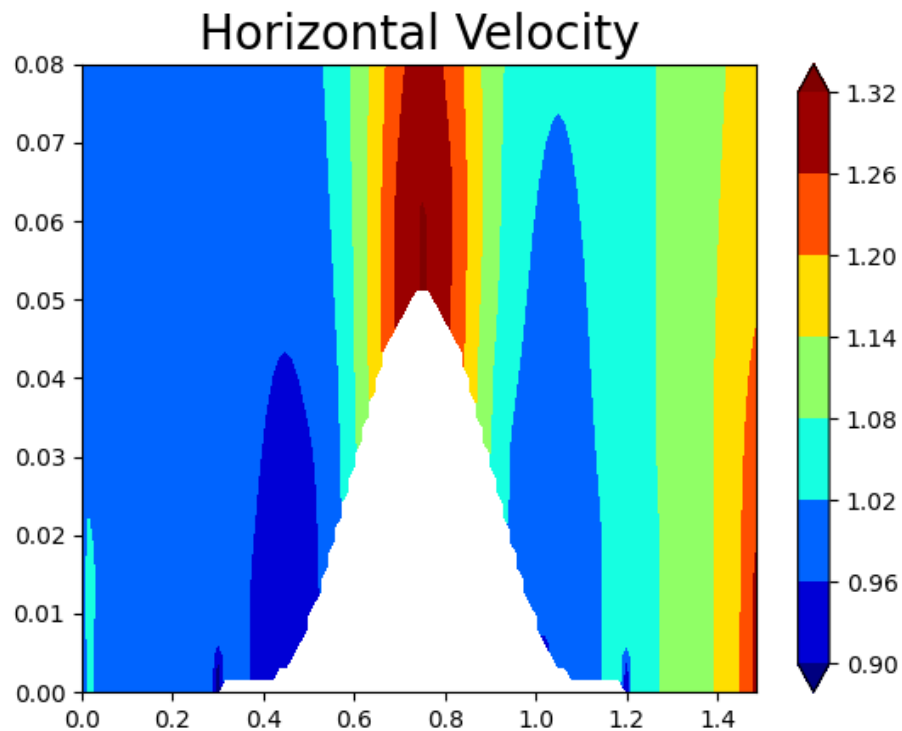


Close-up of the Bump



Maxlevel	Minlevel	y^+ at $x = 0,75$	Number of cells
10	5	1611	~15000
11	5	806	~31000
12	5	403	~52000
13	5	201	~92000

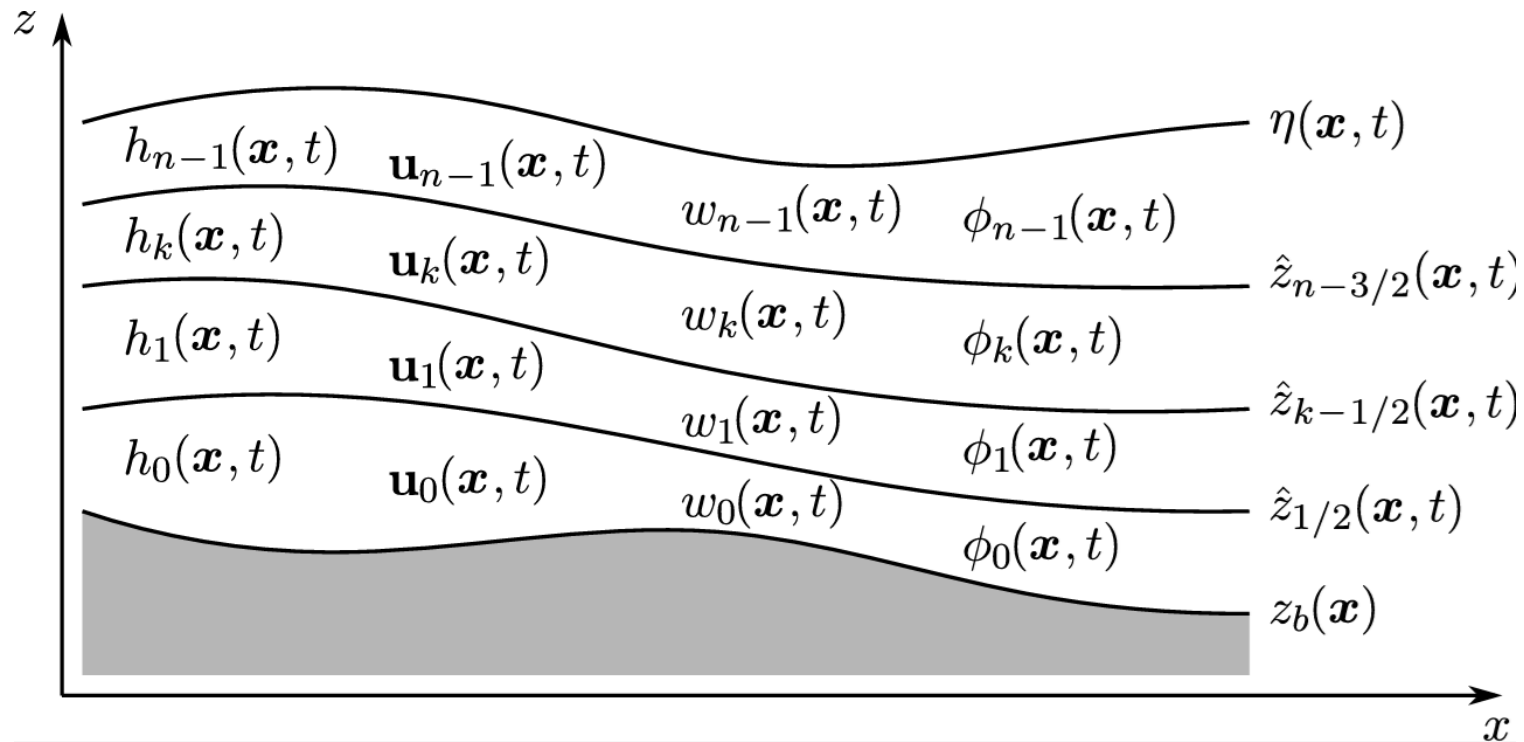
2D Bump in a channel



$$C_f = \frac{\mu \frac{\partial u_t}{\partial y}}{\frac{1}{2} \rho U_0^2}$$

Low Reynolds model

- Use of the multilayer solver : allows elongated mesh close to the solid $\rightarrow$ lower y^+

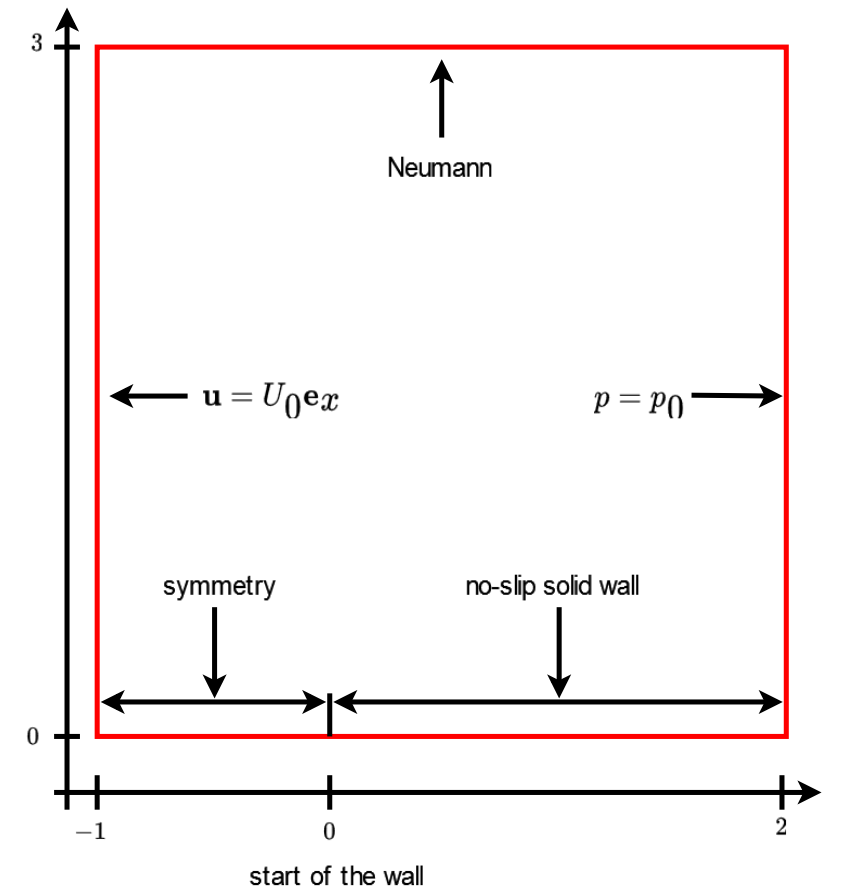


- Low Reynolds model of Chien [1]

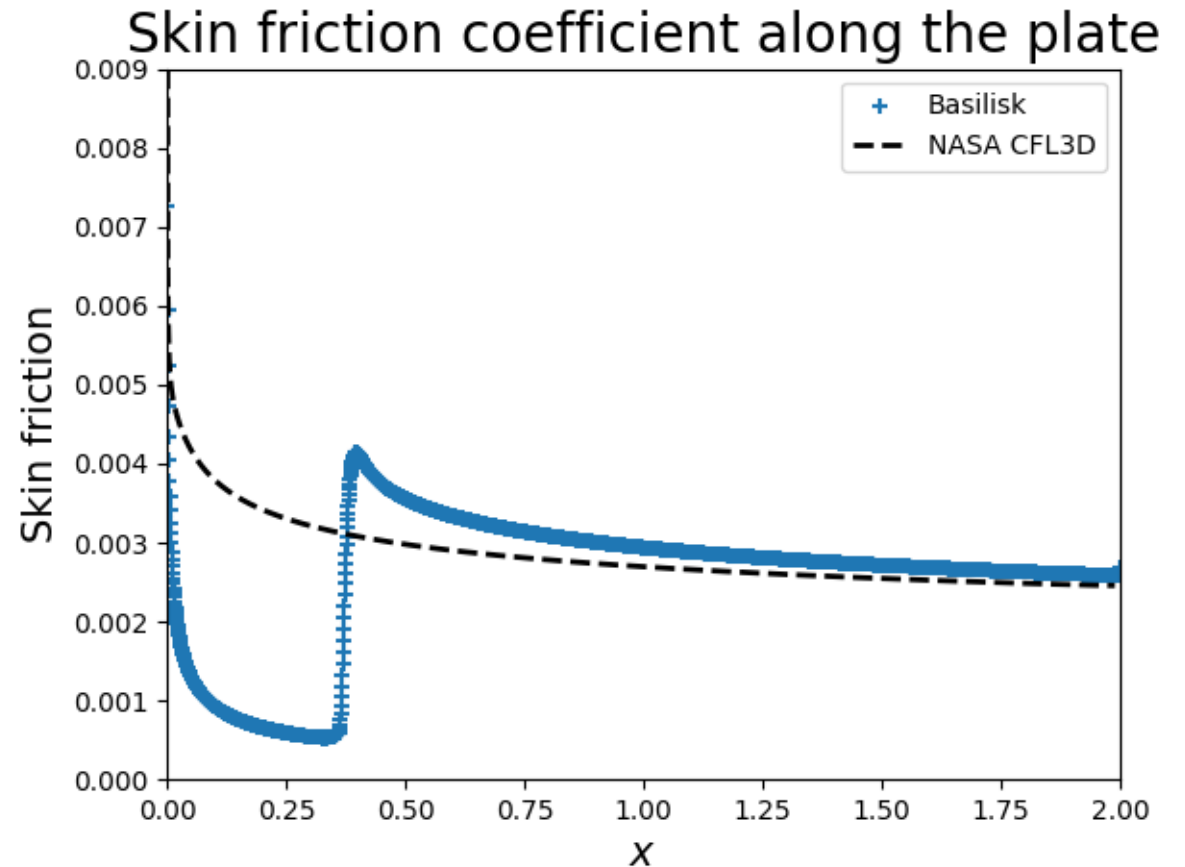
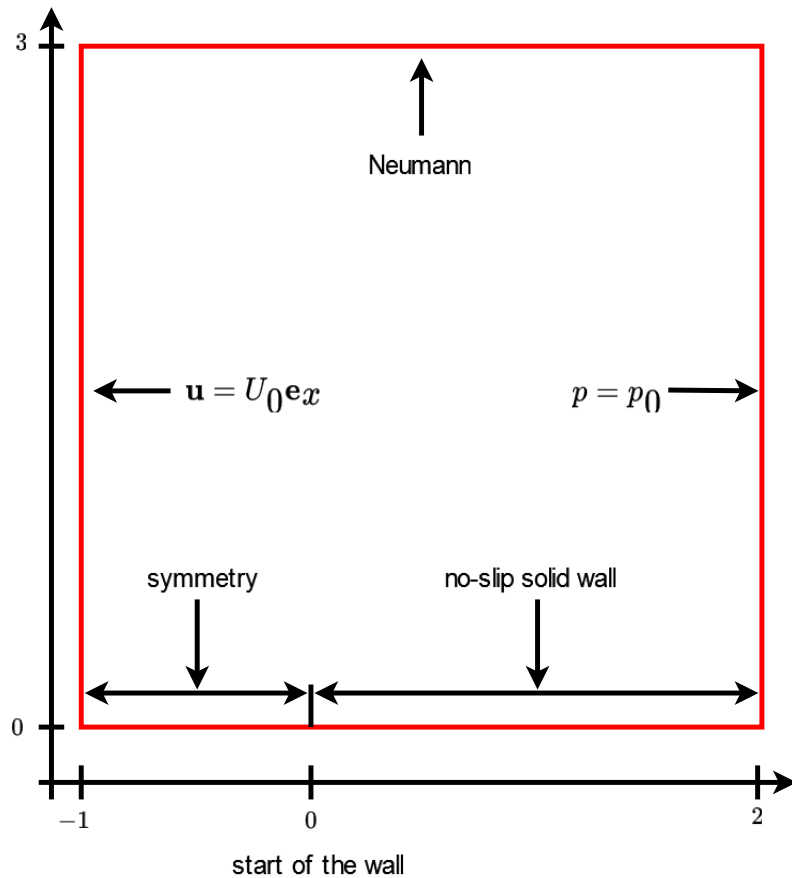
2D Flat Plate with Low Reynolds Model

Same case as for high Reynolds model

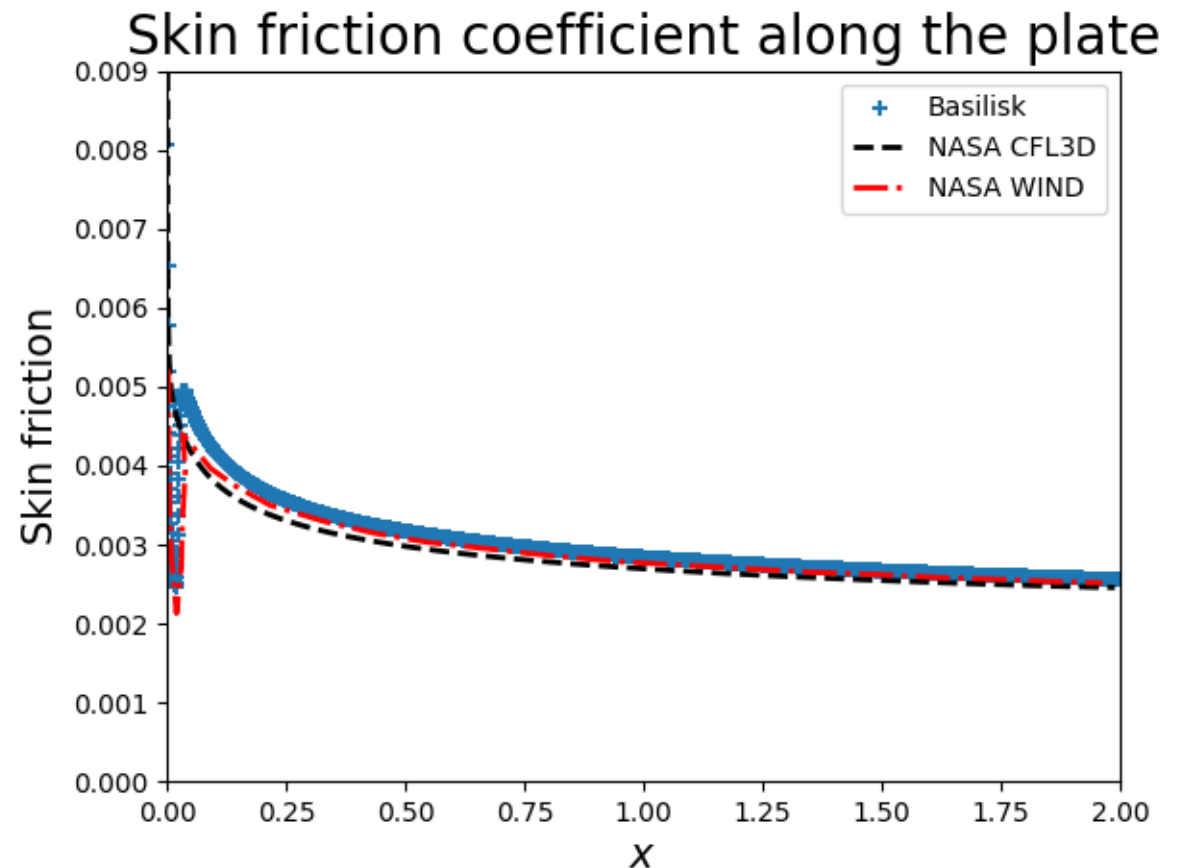
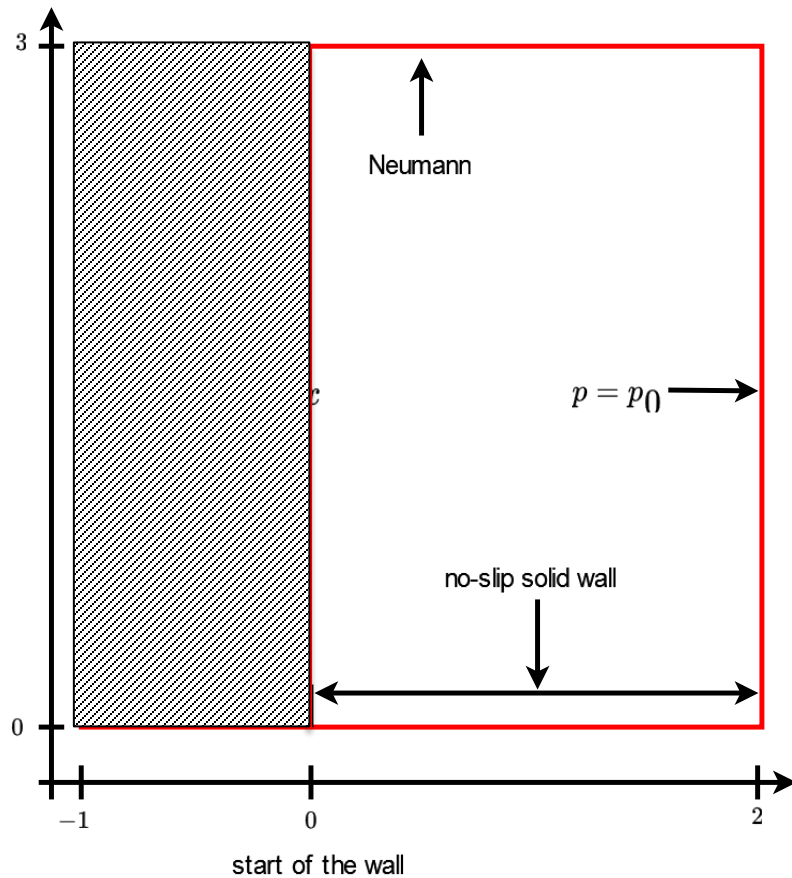
Maxlevel	Minlevel	y^+ at $x = 1$	Number of cells
13	5	68	132028
Multilayer	$nl = 50$ layers	1.2	204800



2D Flat Plate with Low Reynolds Model



2D Flat Plate with Low Reynolds Model



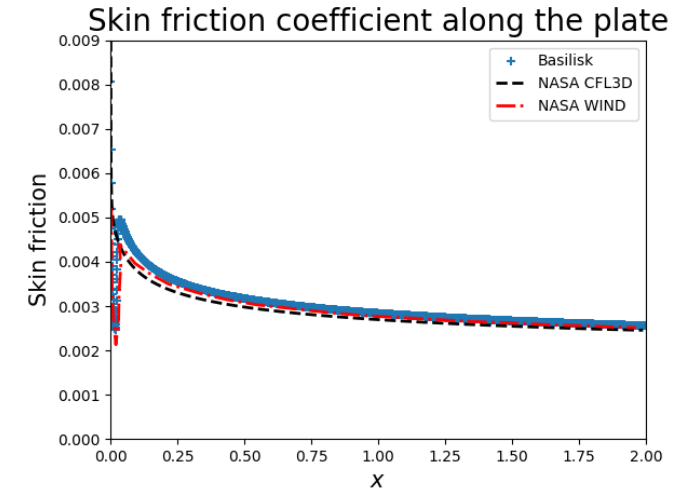
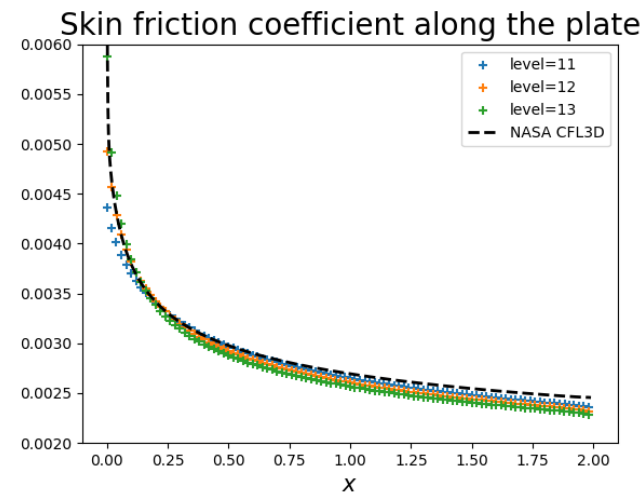
Conclusion and Perspectives

Implementation of a $k - \epsilon$ turbulence model in Basilisk :

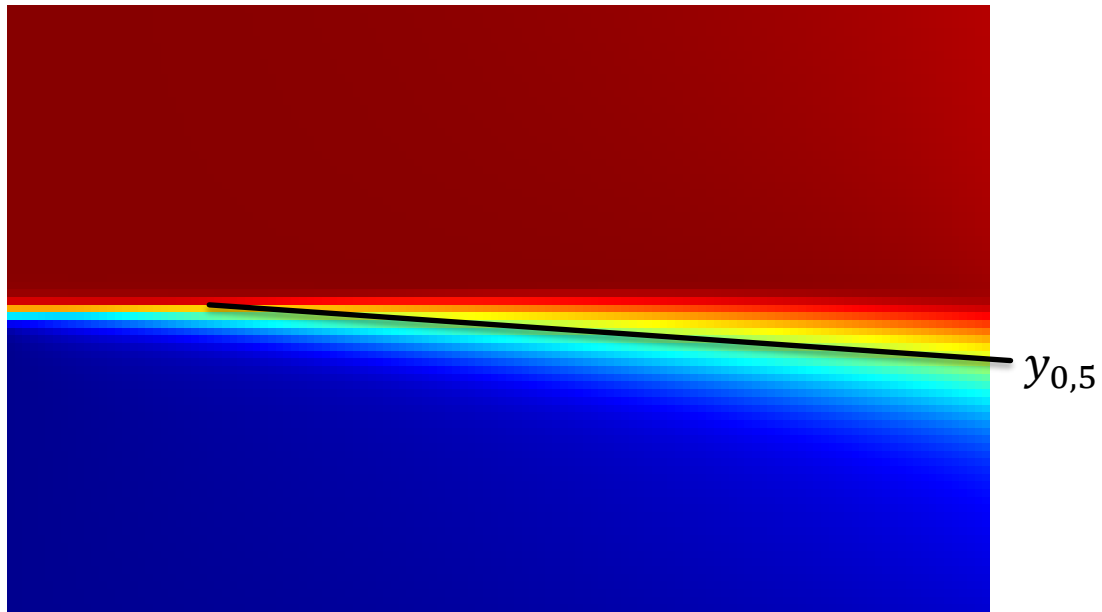
- Good agreement with existing results for the mixing layer and the flat plate with the high-Re model
- More discrepancies for the bump and the flat plate with the low-Re model

What's next : - try different geometries with recirculation zone
- extension to 3D
- Add multiphasics model

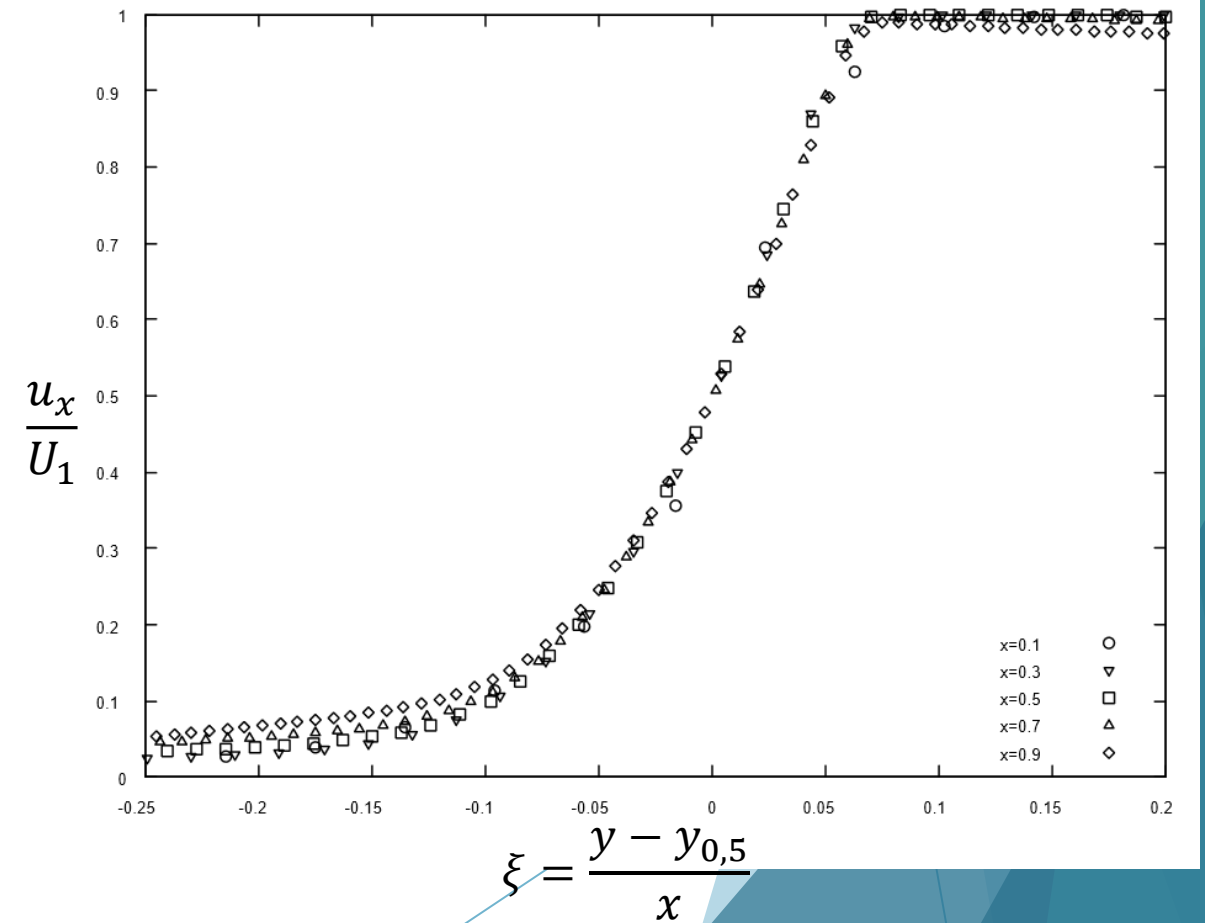
All the codes are available here : [sandbox/aaubert](https://github.com/sandbox/aaubert)



2D Mixing Layer : Self Similarity

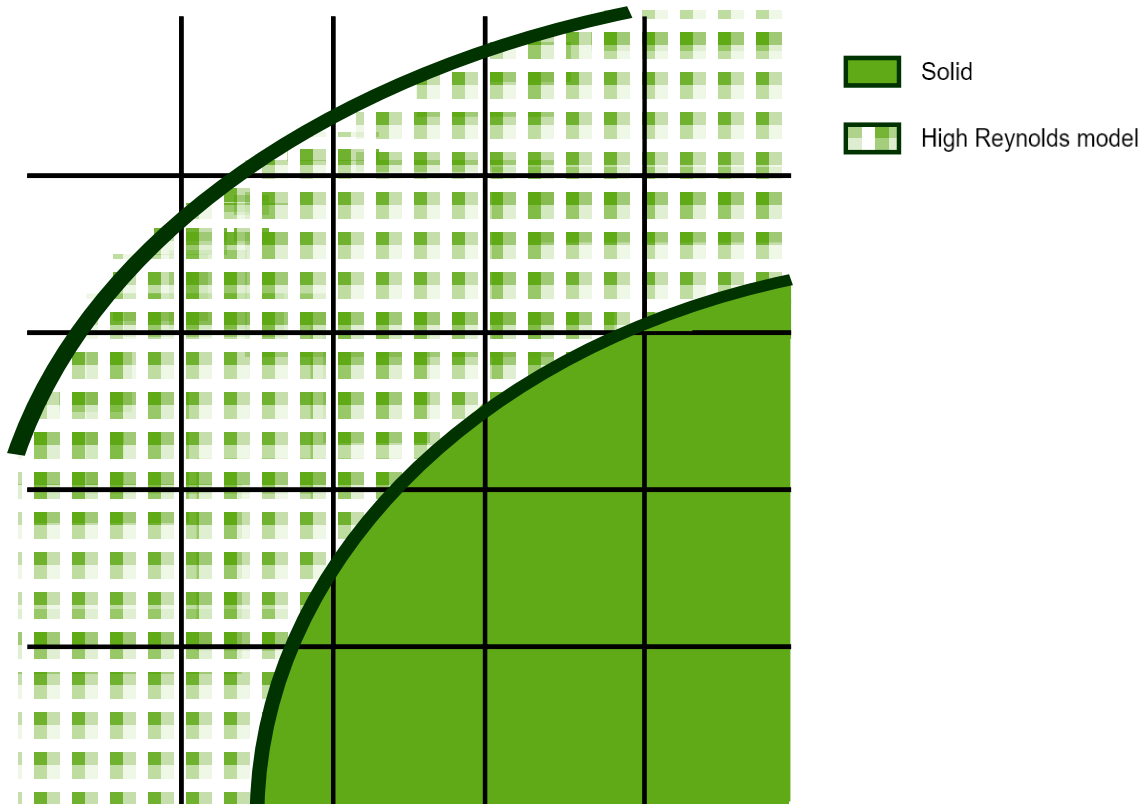


$$u_x(y_{0,5}) = \frac{U_1}{2}$$



High Reynolds model

- Basilisk classical solver uses isotropic mesh : use of high Reynolds model because $y^+ > 30$



Low Reynolds model

- Low Reynolds model of Chien [1]

$$\mu_t = \rho C_\mu f_\mu \frac{k^2}{\epsilon}$$
$$\frac{\partial \rho k}{\partial t} + \frac{\partial \rho k u_i}{\partial x_i} = \frac{\partial}{\partial x_j} \left(\left(\mu + \frac{\mu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right) + P_k - \rho \epsilon - 2 \frac{\mu k}{d^2}$$
$$\frac{\partial \rho \epsilon}{\partial t} + \frac{\partial \rho \epsilon u_i}{\partial x_i} = \frac{\partial}{\partial x_j} \left(\left(\mu + \frac{\mu_t}{\sigma_\epsilon} \right) \frac{\partial \epsilon}{\partial x_j} \right) + C_{1\epsilon} f_1 \frac{\epsilon}{k} P_k - \rho C_{2\epsilon} f_2 \frac{\epsilon^2}{k} - 2 \frac{\mu \epsilon}{d^2} e^{-\frac{d^+}{2}}$$

$$k_{wall} = 0 \text{ and } \epsilon_{wall} = 0$$

$$f_1 = 1, f_2 = 1 - \frac{0.4}{1.8} e^{-\frac{Re_t^2}{36}} \text{ and } f_\mu = 1 - e^{-0.0115 d^+} \text{ with } Re_t = \frac{\rho k^2}{\mu \epsilon}$$

$$C_{1\epsilon} = 1.35, C_{2\epsilon} = 1.80, C_\mu = 0.09, \sigma_k = 1, \sigma_\epsilon = 1.3$$