



# Impact of a drop containing a bubble



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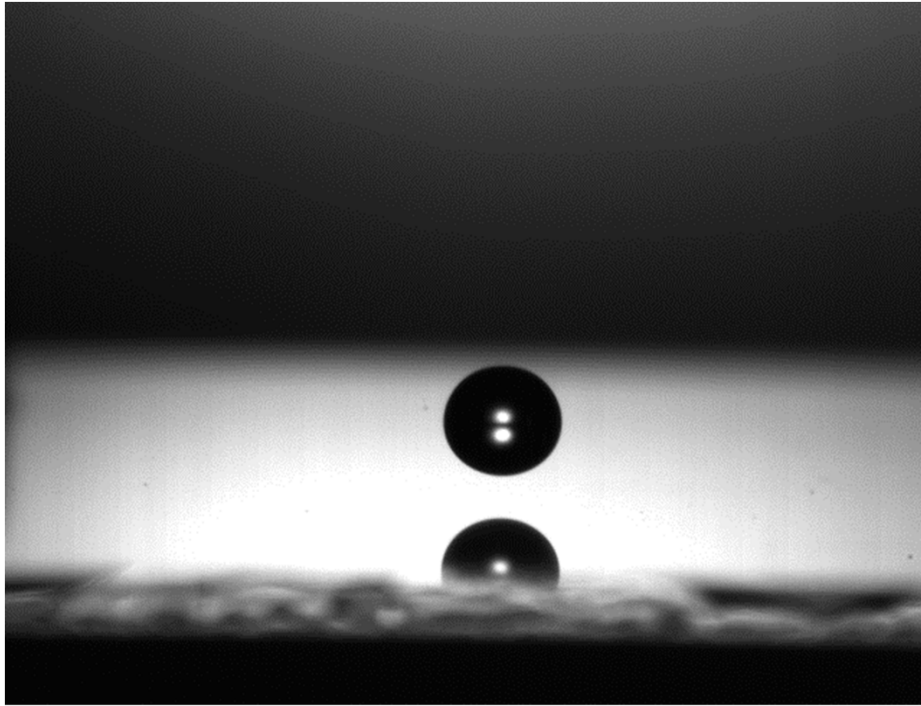
– 机械结构强度与振动国家重点实验室

Xi'an Jiaotong University – 西安交通大学

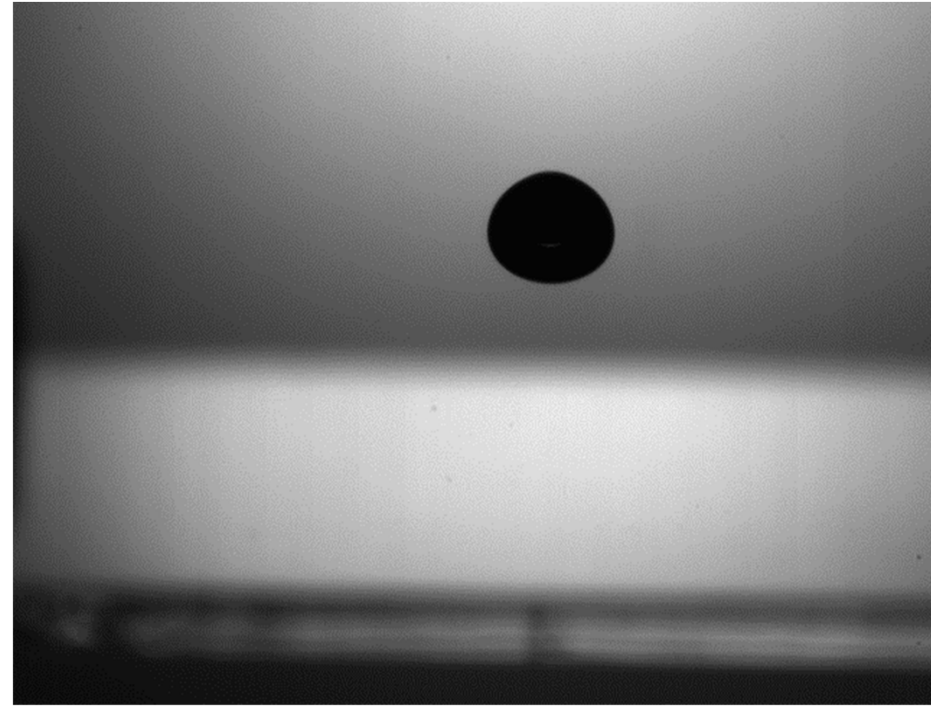


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for Applied Mechanics

# Vertical splashing

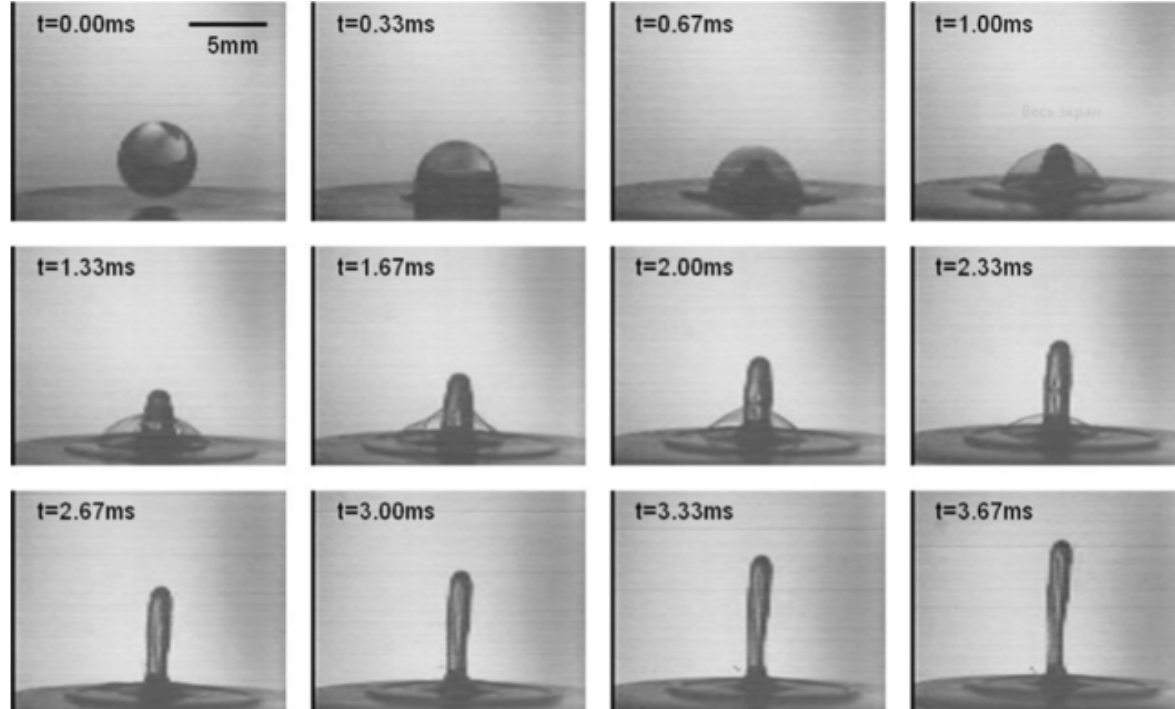
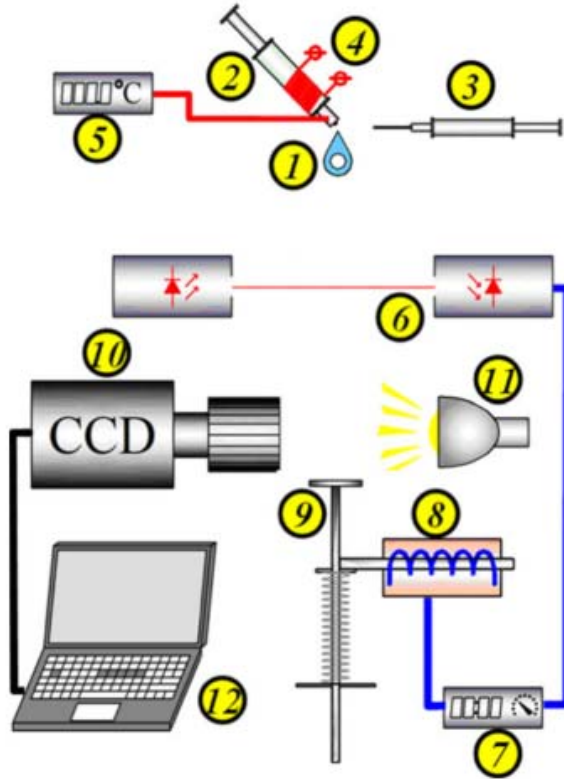


Silicone Oil 10 cSt  
45 cm

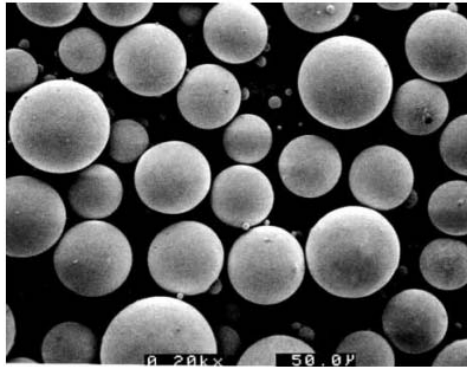


Silicone Oil 10 cSt  
150 cm

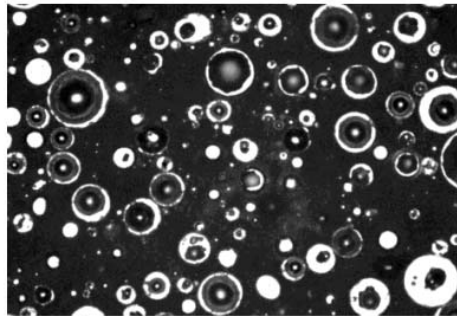
# Previous observations



# Thermal Barrier Coatings

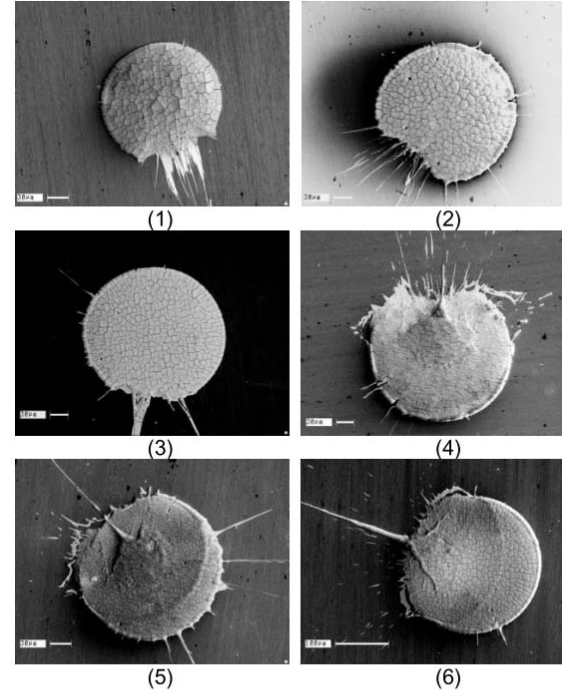


(a)



(b)

**Fig. 3.** SEM photos of the hollow spherical particles of a specially prepared YSZ powder. (a) – general view of the particles, (b) – cross-sectional cut of the particles.



**Fig. 4.** Irregular YSZ splats formed as a consequence of jet gas emission at the periphery of flattening hollow droplet.

Solonenko, O. P., Mikhilchenko, A. A., & Kartaev, E. V. (2005). Splat formation under YSZ hollow droplet impact onto substrate. In *Proceedings of the International Thermal Spray Conference (ITSC-2005)* (pp. 1–6). Basel, Switzerland: ASM International.

# Previous observations

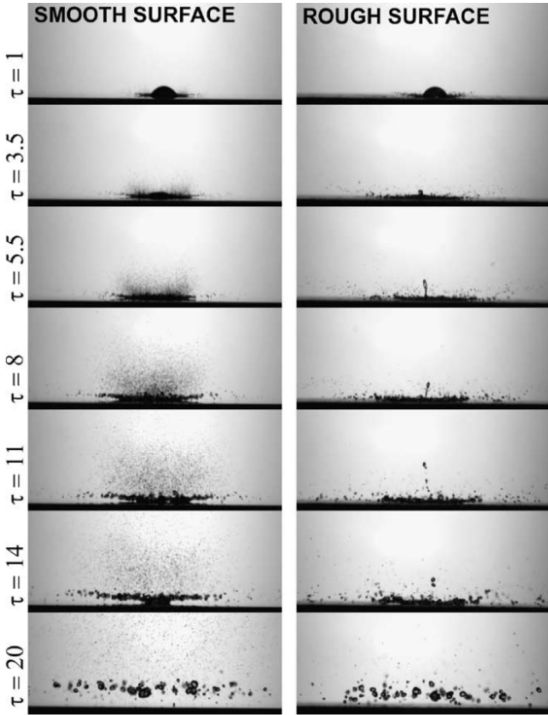


Fig. 6. Time evolution of water drop impact onto smooth (S) and rough (R) surfaces at 260 °C; pure water:  $Ca = 0.0431$ ,  $La = 133,000$ ,  $We = 247$ .

Cossali, G. E., Marengo, M., & Santini, M. (2005). Secondary atomisation produced by single drop vertical impacts onto heated surfaces. *Experimental Thermal and Fluid Science*, 29(8), 937–946.

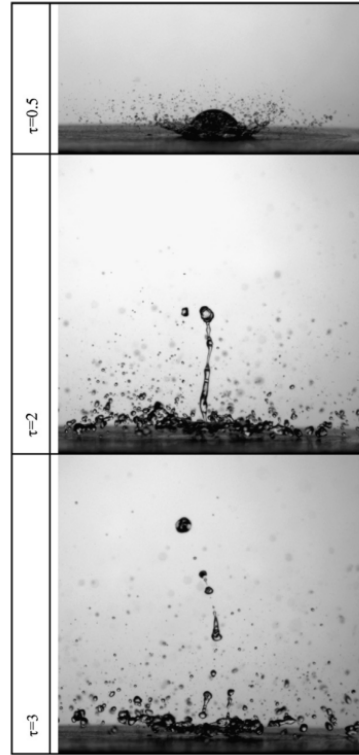


Fig. 4. Impact of a drop under *film boiling* regime ( $T_w = 260$  °C,  $R_c = 14.5$  μm,  $We = 285$ ,  $Ca = 0.046$ ).

Cossali, G. E., Marengo, M., & Santini, M. (2008). Thermally induced secondary drop atomisation by single drop impact onto heated surfaces. *International Journal of Heat and Fluid Flow*, 29(1), 167–177.

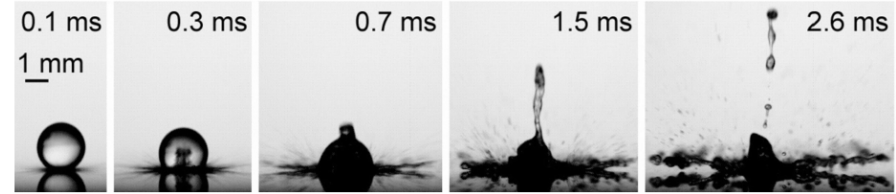


Fig. 7. Central jet of the 5.21% NaCl solution drop with  $T_w = 384$  °C and  $We = 41$ .

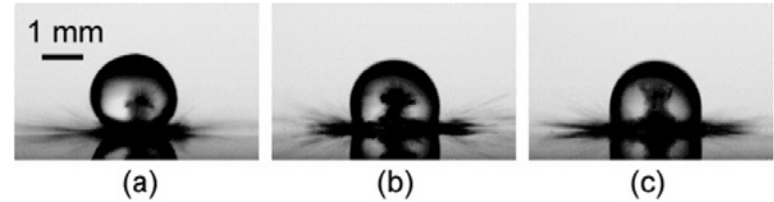
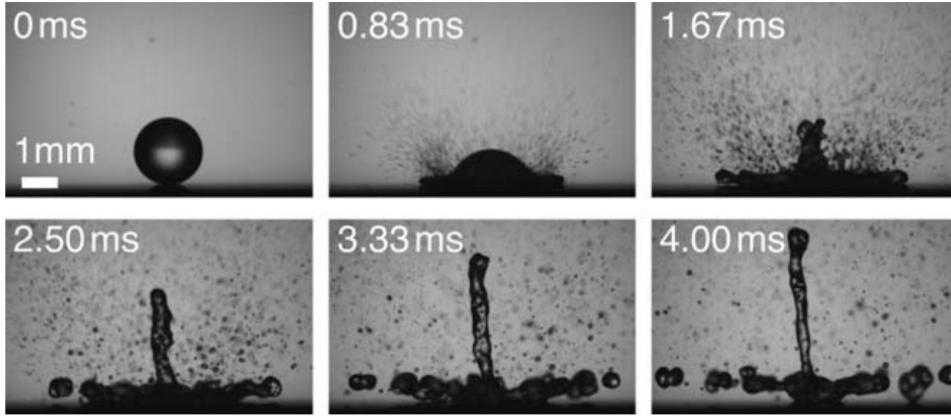


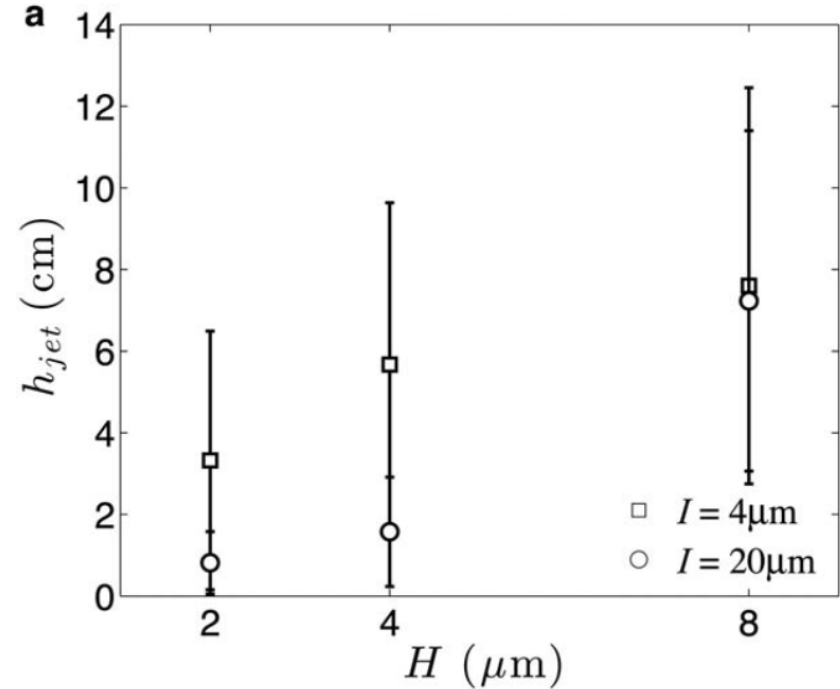
Fig. 8. Initial stage after the 5.21% NaCl solution drop impact with  $T_w = 384$  °C, (a)  $We = 2$ , (b)  $We = 22$  and (c)  $We = 130$ .

Liang, G., Shen, S., Guo, Y., & Zhang, J. (2016). Boiling from liquid drops impact on a heated wall. *International Journal of Heat and Mass Transfer*, 100, 48–57.

# Previous observations



**Fig. 11** Jet formation during the impact of a water droplet on a structured surface ( $l = 4 \mu\text{m}$ ,  $H = 2 \mu\text{m}$ ) heated to  $300^\circ\text{C}$ . The diameter of the drop is  $2.2 \text{ mm}$ , and the impact velocity is  $1.3 \text{ m s}^{-1}$ .



Tran, T., Staat, H. J. J., Susarrey-Arce, A., Foertsch, T. C., van Houselt, A., Gardeniers, H. J. G. E., Prosperetti, A., Lohse, D., Sun, C. (2013). Droplet impact on superheated micro-structured surfaces. *Soft Matter*, 9(12), 3272–3282.

# Hollow sphere model

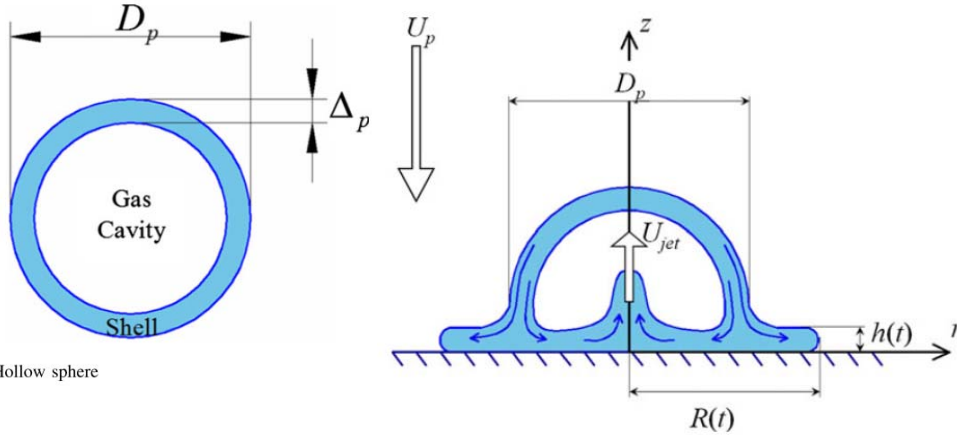


Fig. 1 Hollow sphere

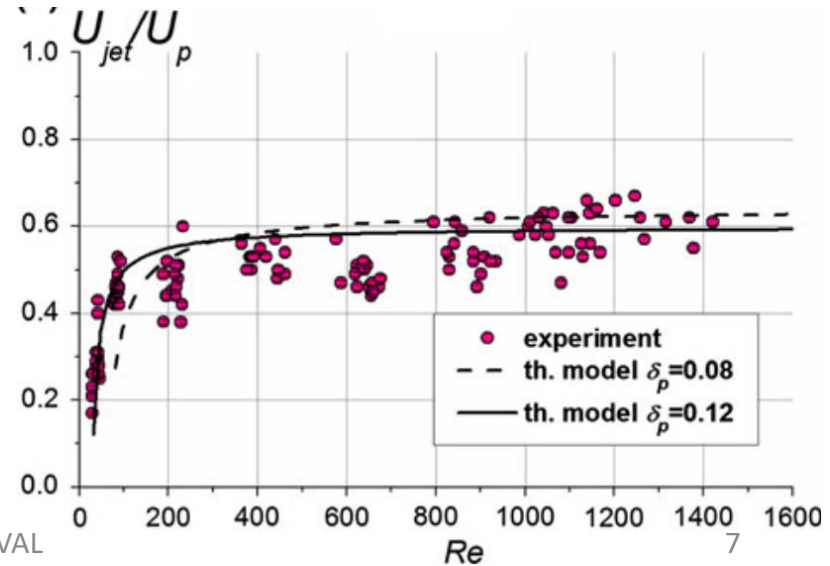
$$\frac{U_{jet}}{U_p} = \sqrt{A(\delta_p) \left(1 - \frac{B(\delta_p)}{Re}\right)},$$

$$\text{where } A(\delta_p) = 1 - \frac{3\delta_p}{1 - (1 - 2\delta_p)^3}, \quad B(\delta_p) = \frac{3}{4\delta_p} \cdot \frac{1}{1 - (1 - 2\delta_p)^3 - 3\delta_p}.$$

$$Re = \rho D_p U_p / \mu$$

$$We = \rho D_p U_p^2 / \sigma$$

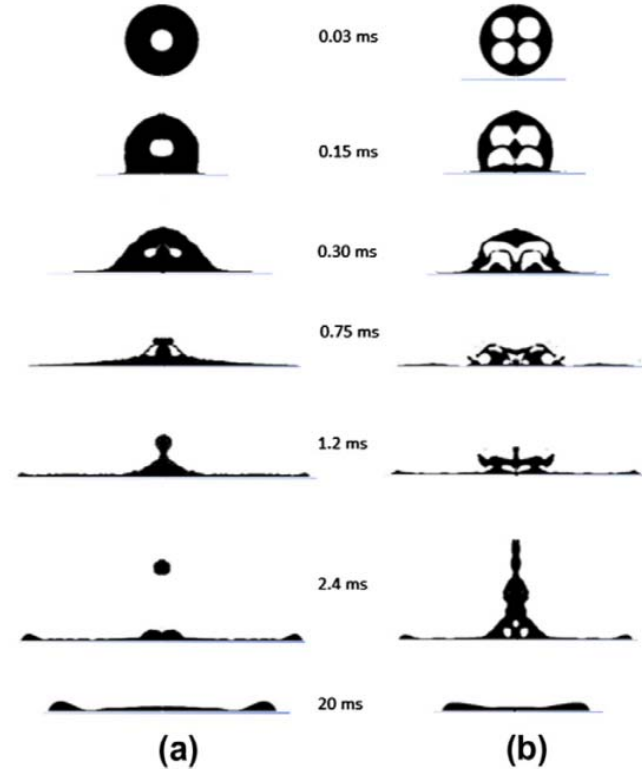
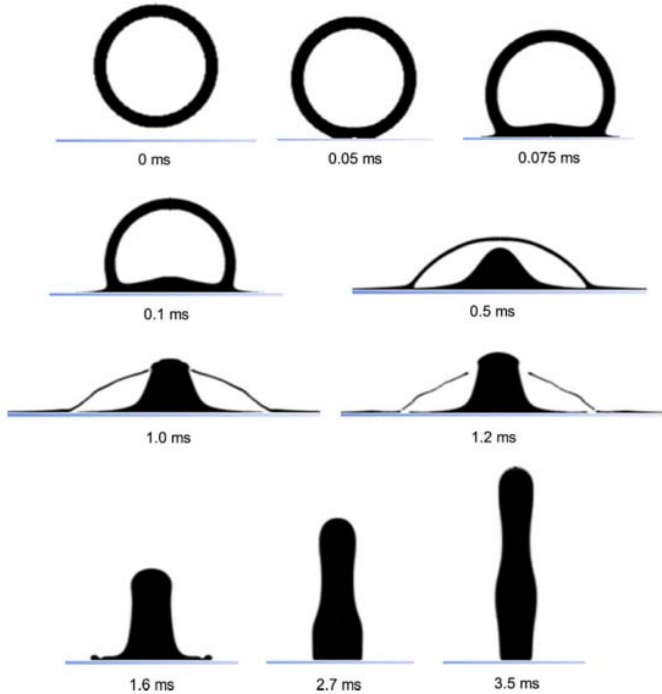
$$\delta_p = \Delta_p / D_p$$





# Previous simulations

“two-dimensional axisymmetric formulation”



**Fig. 6.** Snapshots of droplet spreading for different void fraction (a) hollow droplet ( $d/D_0 = 0.3$ ) and (b) hollow droplet with four small distributed voids having the same mass as that of  $d/D_0 = 0.5$  hollow droplet.

Kumar, A., Gu, S., & Kamnis, S. (2012). Simulation of impact of a hollow droplet on a flat surface. *Applied Physics A*, 109(1), 101–109.

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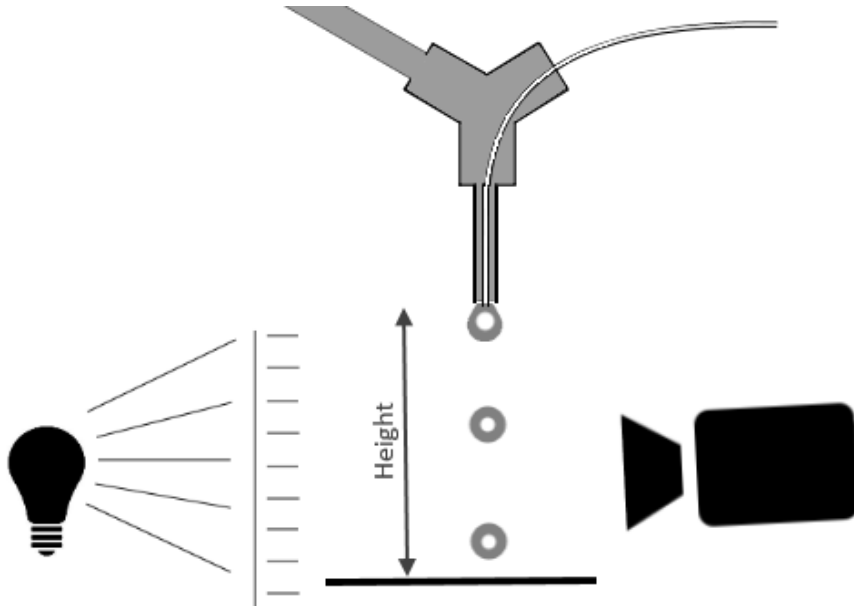
Kumar, A., & Gu, S. (2012). Modelling impingement of hollow metal droplets onto a flat surface. *International Journal of Heat and Fluid Flow*, 37, 189–195.



# Outline

1. Preliminary experiments in Twente
2. Numerical simulations (Gerris):
  - a) Impact velocity
  - b) Bubble size
  - c) Bubble vertical position / Film thickness
  - d) Liquid properties

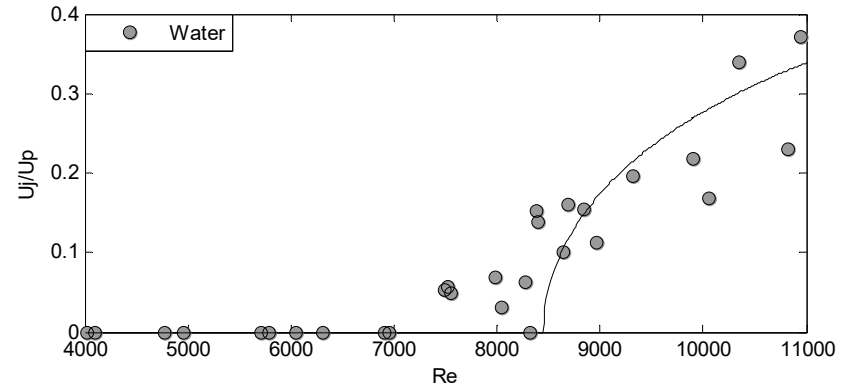
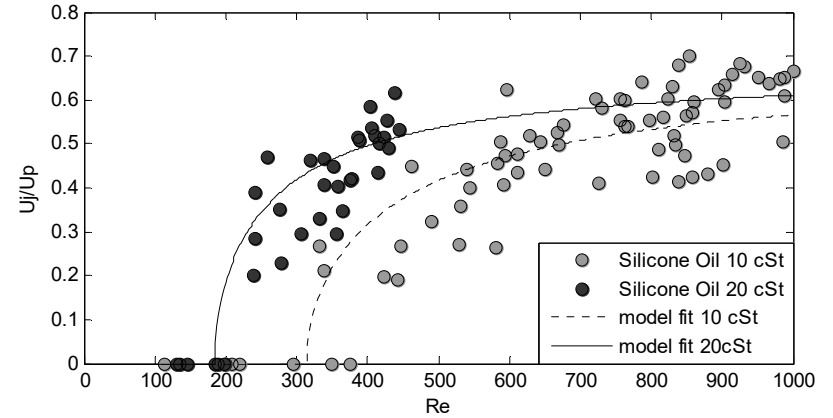
# 1. Preliminary experiments in Twente



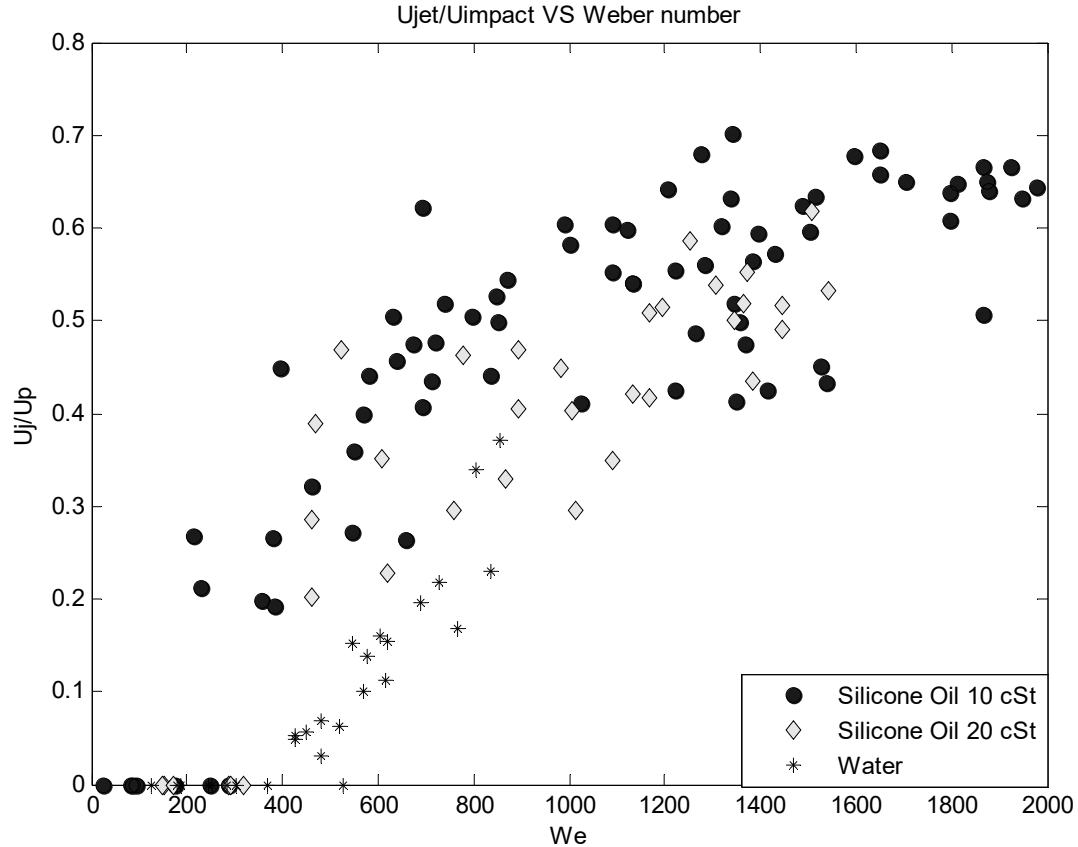
$\delta_p = 0.03$  Silicone oil 10 cSt (estimated  $\delta_p = 0.25$ )

$\delta_p = 0.04$  Silicone oil 20 cSt (estimated  $\delta_p = 0.31$ )

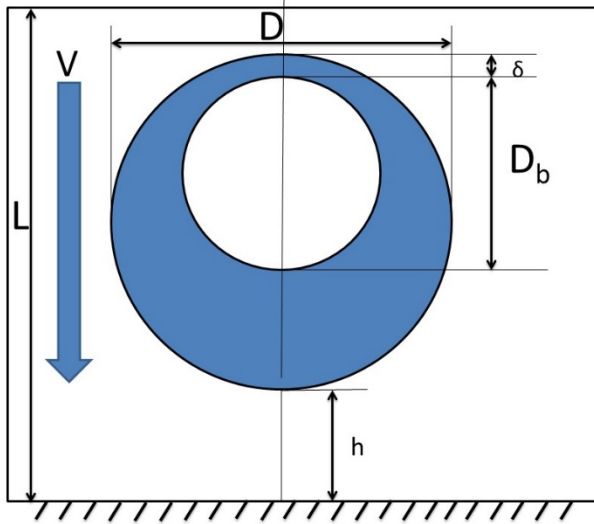
$\delta_p = 0.0055$  Water (estimated  $\delta = 0.25$ )



# Jet velocity



## 2. Numerical simulations (Gerris)

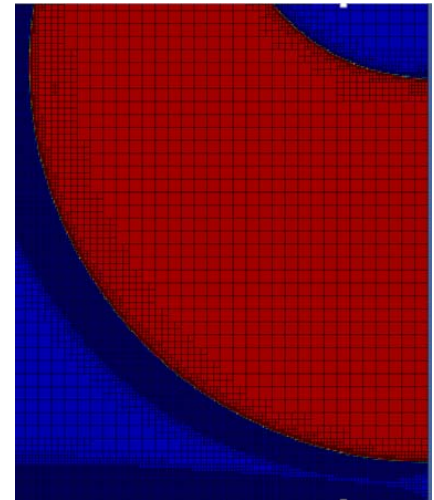
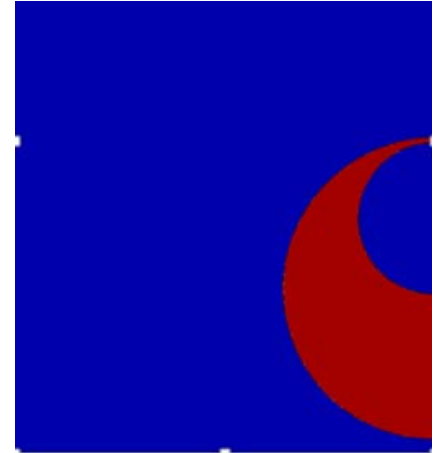


$D_b^*$	$D_b/D$
$\delta^*$	$\delta/D$
$V_j$	Maximum jet velocity
$v_j$	Jet velocity
$V_j^*$	$V_j/V$
$v_j^*$	$v_j/V$
$P^*$	$P/\rho V^2$
$\nabla P^*$	$\delta p^*/\delta z$

Level of refinement: 10 ( $2^{10}$  cells in each direction)

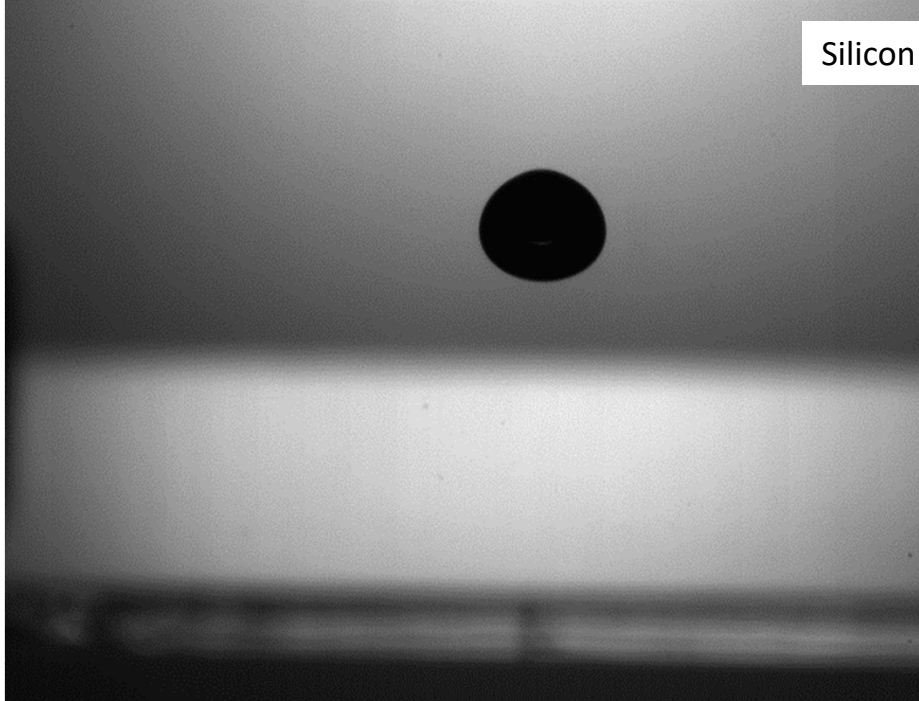
->  $2^{10} \cdot D/L = 491$  cells per drop diameter

$L/D = 2.08$ ,  $h/D = 0.478$

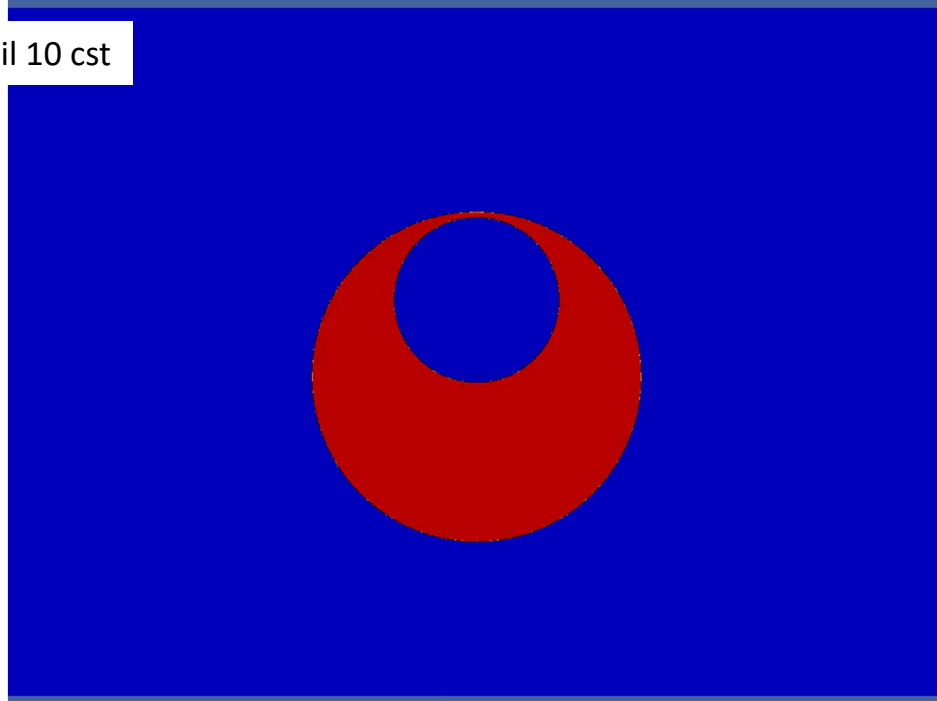


# Validation

$D_b^*$	$D_b/D$
$\delta^*$	$\delta/D$



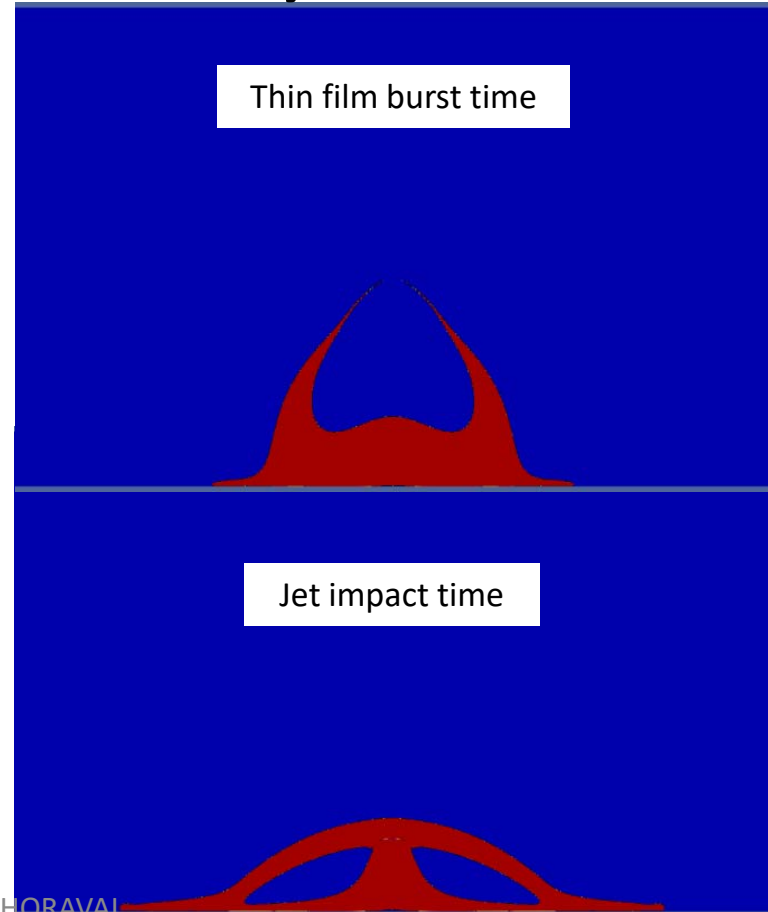
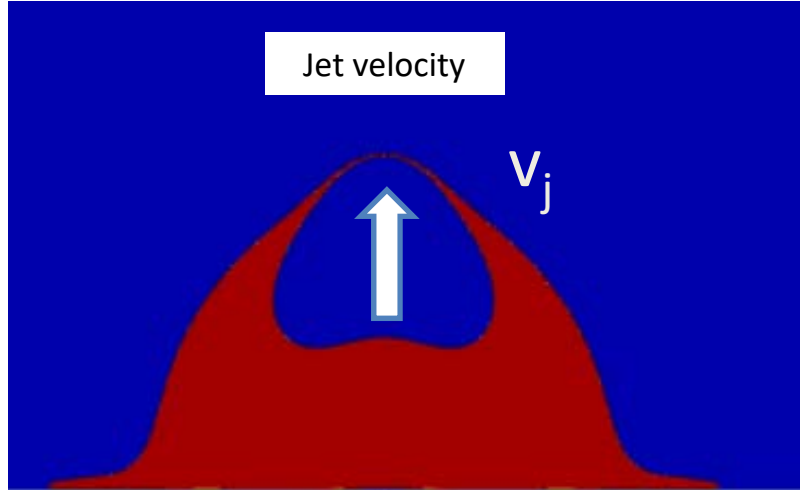
Silicon oil 10 cst



$D = 2.75 \text{ mm}$ ,  $V = 4.59 \text{ m/s}$

$D = 2.75 \text{ mm}$ ,  $V = 4.59 \text{ m/s}$ ,  
 $\delta^* = 0.0175$ ,  $D_b^* = 0.5$ ,  $Re = 1010$

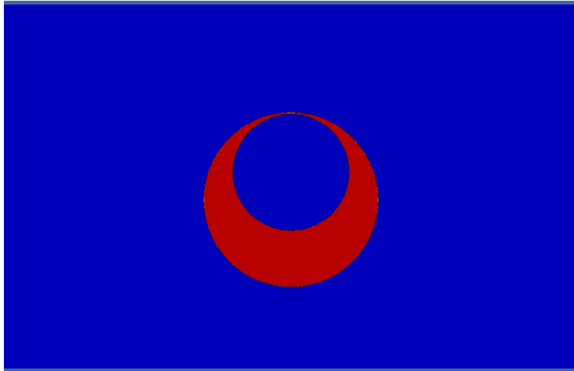
# Quantitative analysis



# Bursting and impact times

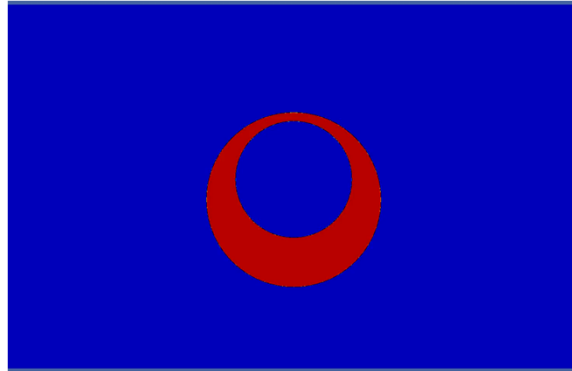
Typical cases of different results on film bursting and impacting of jet and film

Film bursts before maximum jet velocity happens.



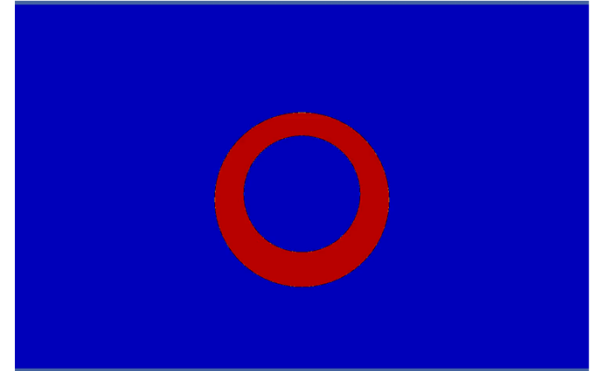
$\delta^* = 0.01$ ,  $V=4.276$  m/s,  $D_b^* = 0.67$

Film bursts after maximum jet velocity happens.



$\delta^* = 0.05$ ,  $V=4.276$  m/s,  $D_b^* = 0.67$

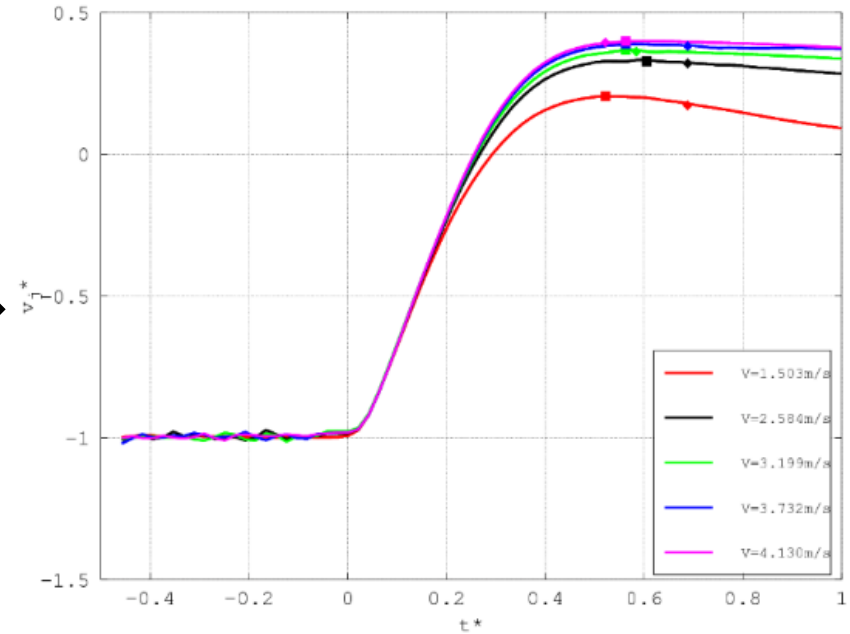
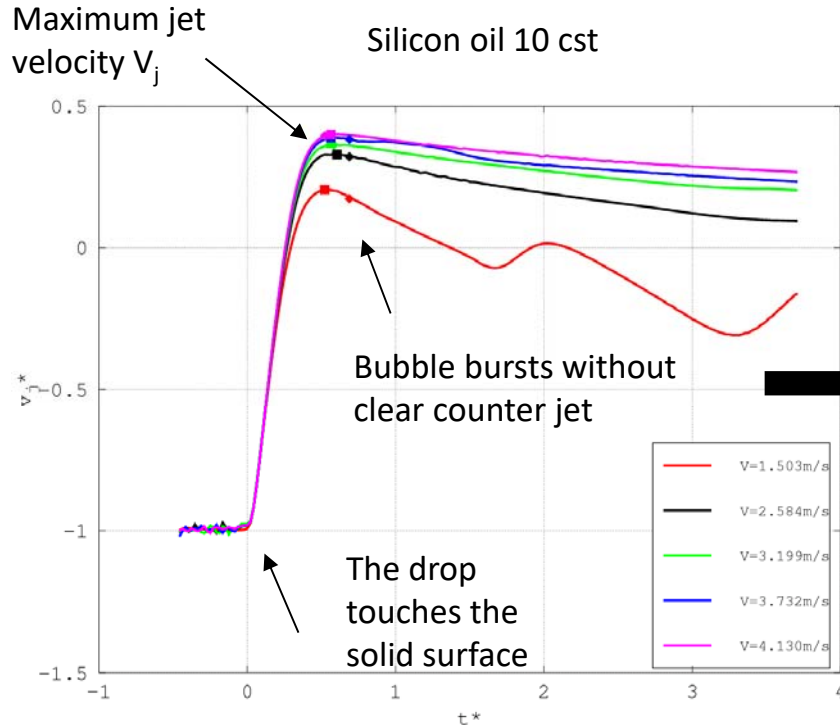
The jet impacts the film before it breaks.



$\delta^* = 0.13$ ,  $V=4.276$  m/s,  $D_b^* = 0.67$



# 2a) Impact velocity



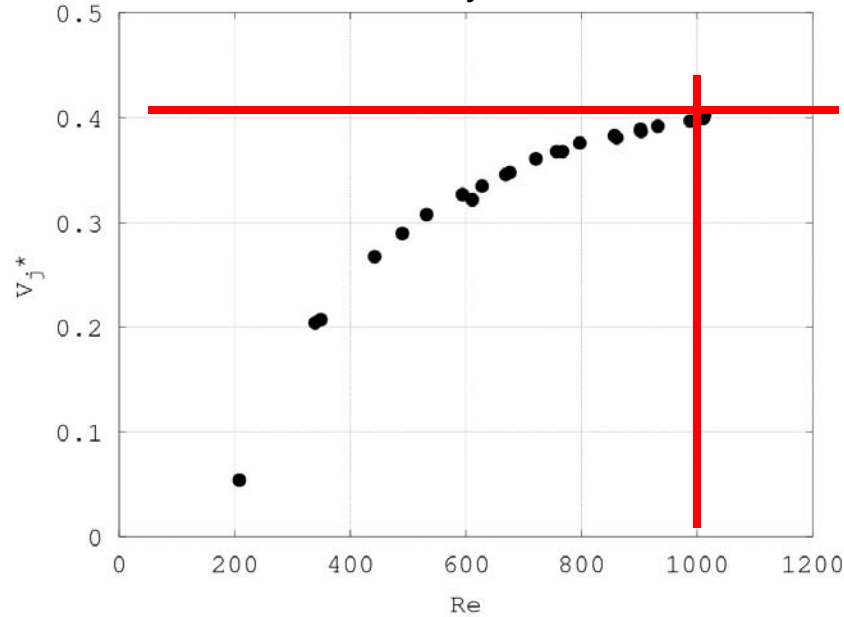
■ Maximum jet velocity time

● Burst time

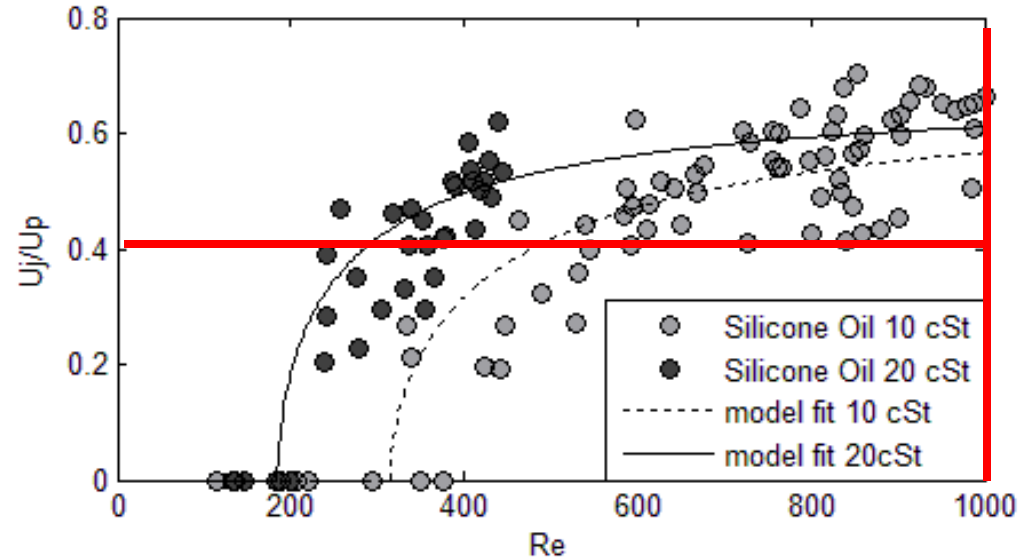
$V = 1.50 \text{ m/s}, 2.58 \text{ m/s}, 3.19 \text{ m/s}, 3.73 \text{ m/s}$  and  $4.13 \text{ m/s}$ .  
 $D = 2.75 \text{ mm}, \delta^* = 0.0175, D_b^* = 0.5$ .

# 2a) Impact velocity

Max  $V_j \sim 0.4$



Max  $V_j \sim 0.7$



Simulations for Silicon oil 10 cst  
 $D = 2.75$  mm,  $\delta^* = 0.0175$ ,  $D_b^* = 0.5$

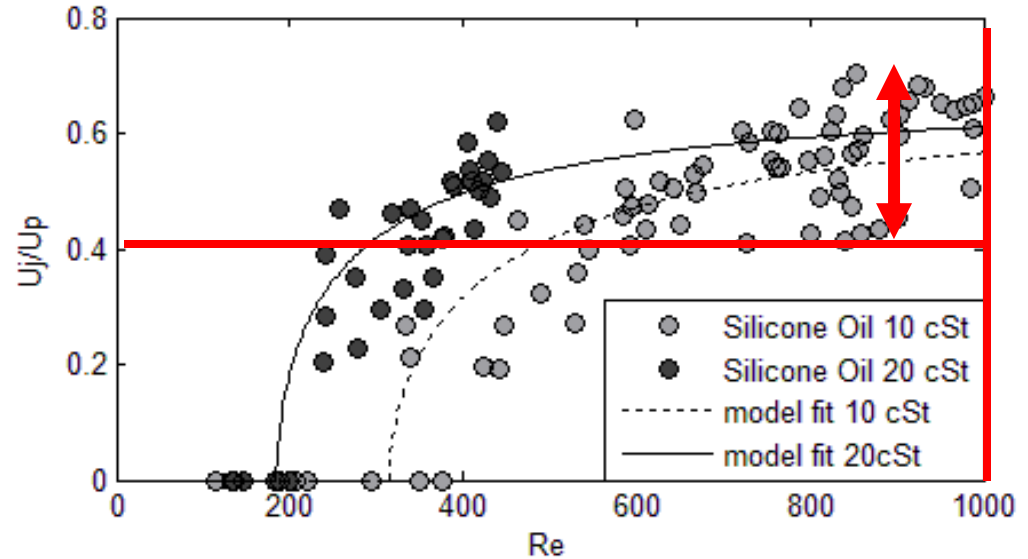
Experiments  
PoF, University of Twente (2014)

# Origin of the dispersion

Strong dispersion in experiments

Hypothesis:

- Bubble size
- Bubble vertical position
- Compressible effects
- Non-axisymmetry
- Bubble and drop shape
- ...?



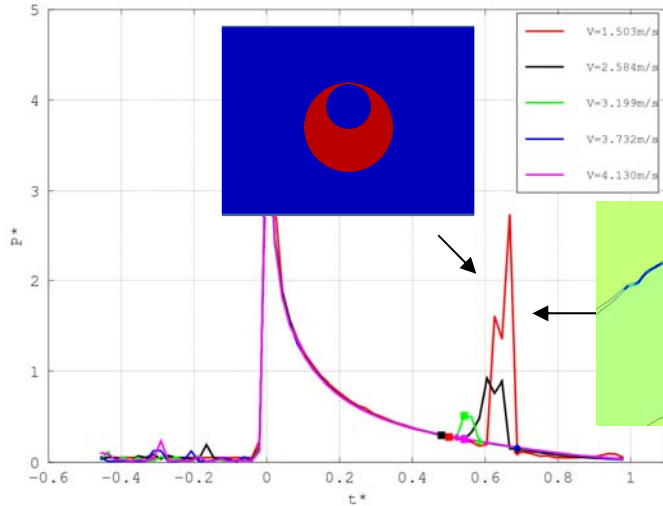
Experiments  
PoF, University of Twente (2014)

# 2a) Impact velocity

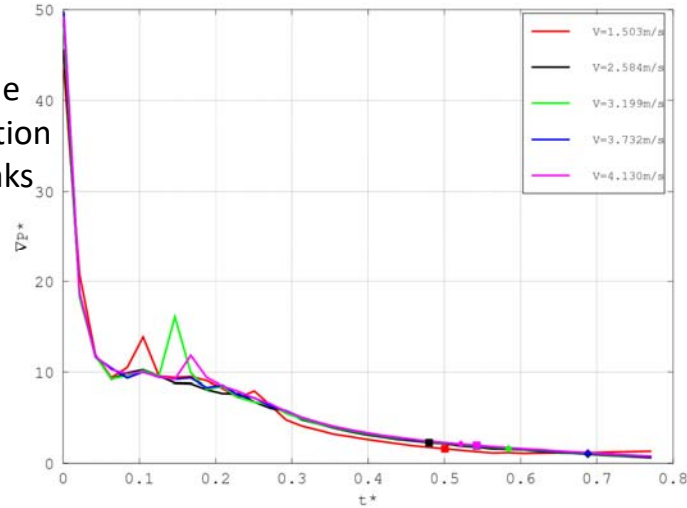
Maximum pressure on axis

Silicon oil 10 cst

Maximum vertical pressure gradient on axis



The jump is because of the film deformation before it breaks



● Burst time

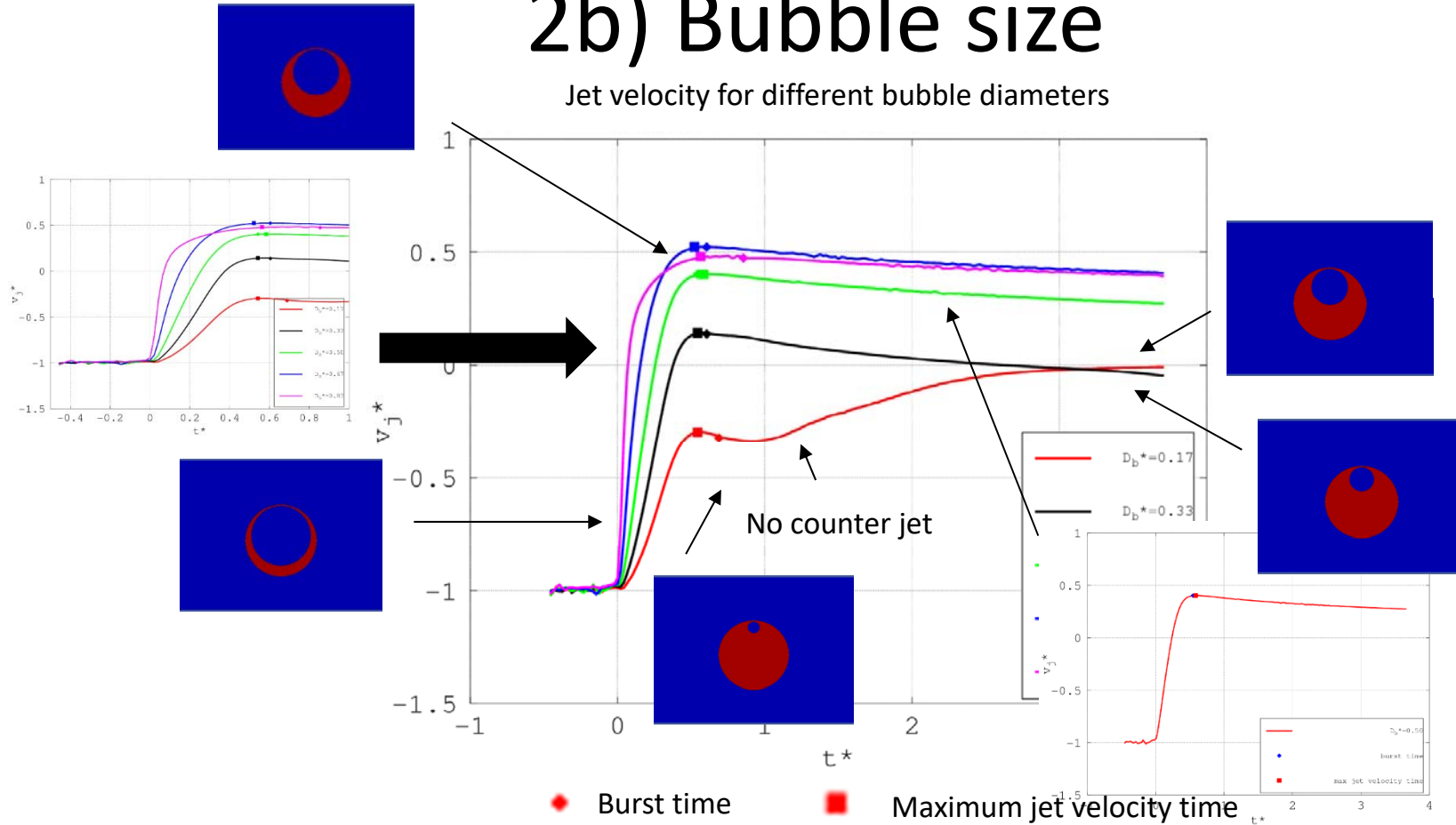
■ Maximum jet velocity time

$V = 1.50\text{m/s}, 2.58\text{m/s}, 3.19\text{m/s}, 3.73\text{m/s}$  and  $4.13\text{m/s}$ .  $D = 2.752\text{mm}$ ,  $\delta^* = 0.0175$   $D_b^* = 0.5$ .

Impact velocity has little effect on non-dimensional pressure and non-dimensional pressure gradient.

# 2b) Bubble size

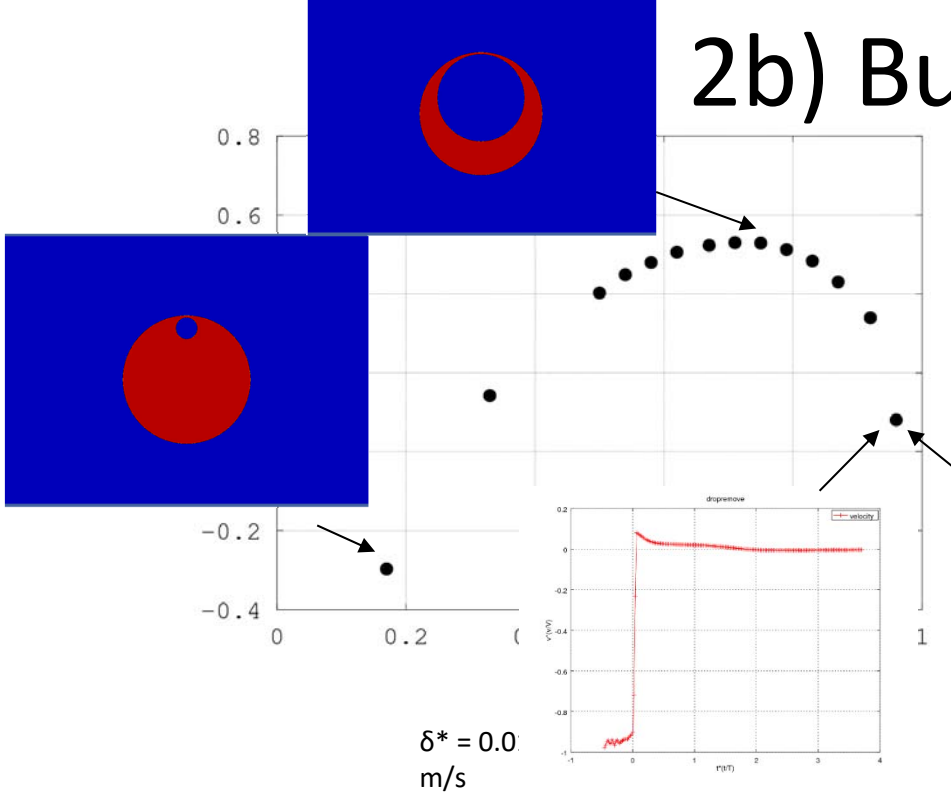
Jet velocity for different bubble diameters



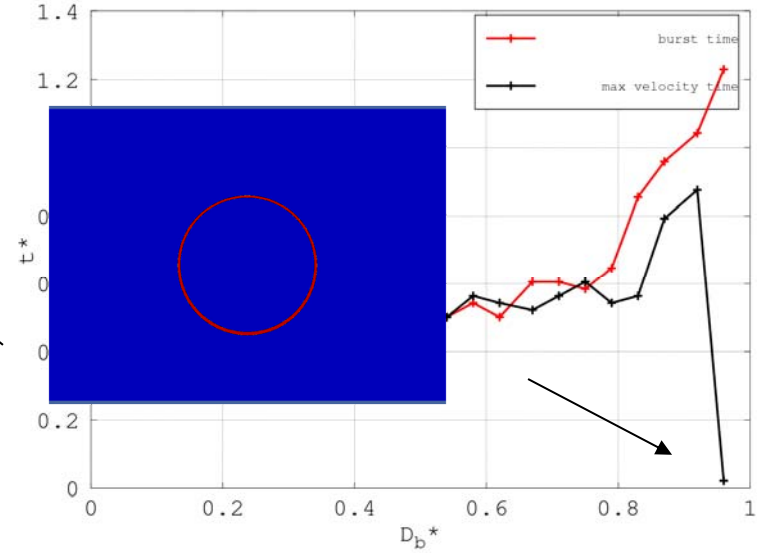
$\delta^* = 0.017$ ,  $V = 4.276$  m/s,  $D_b^* = 0.17, 0.33, 0.50, 0.67, 0.83$ .

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## 2b) Bubble size



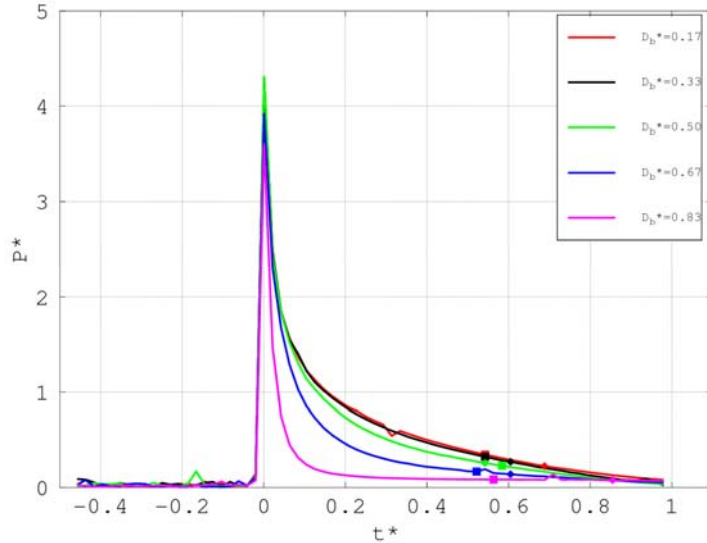
The relation between maximum jet velocity and bubble diameter. The max jet velocity can reach  $0.55V$  at  $D_b^* = 0.63$ . The max jet velocity is close to the experiment results.



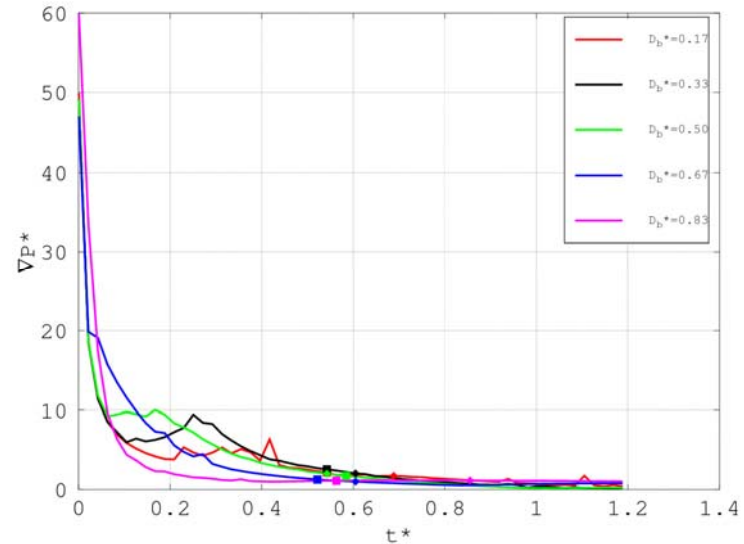
Time scaling of burst of thin film and maximum jet velocity

# 2b) Bubble size

Maximum pressure on axis



Maximum vertical pressure gradient on axis



● Burst time

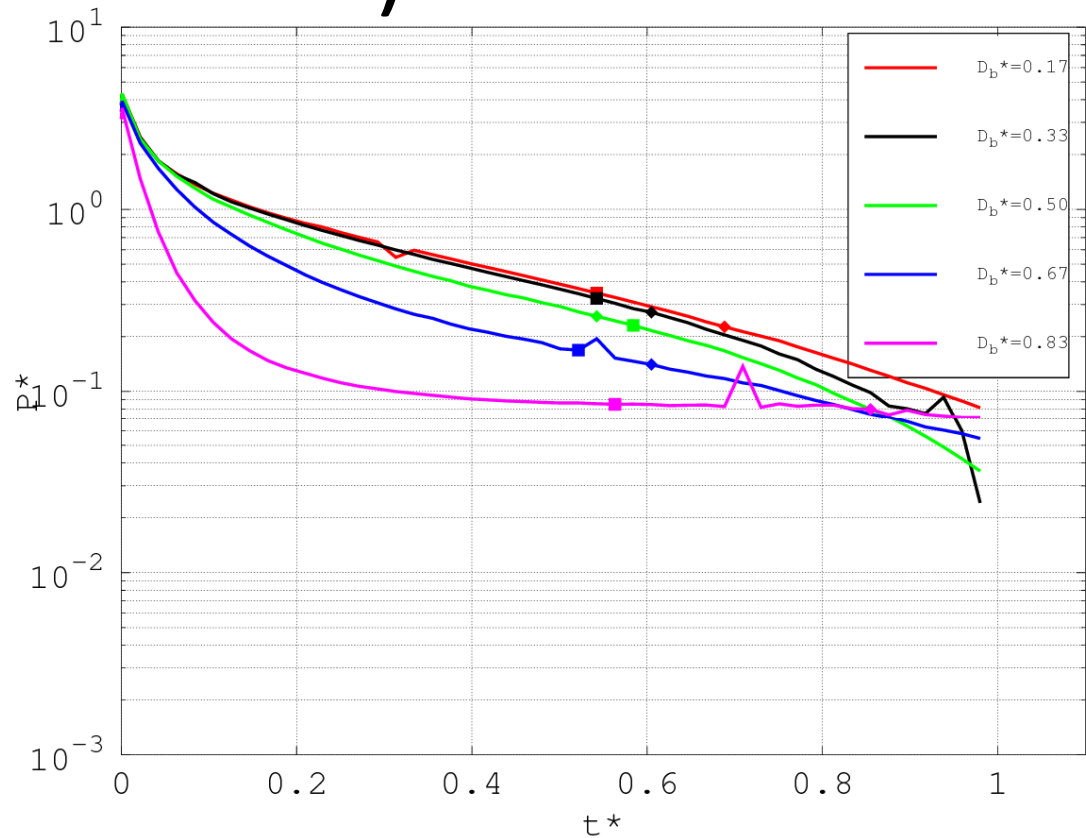
■ Maximum jet velocity time

$\delta^* = 0.017$ ,  $V = 4.276$  m/s,  $D_b^* = 0.17, 0.33, 0.50, 0.67, 0.83$ .

Bubble size has significant effect on non-dimensional pressure and non-dimensional pressure gradient



# 2b) Bubble size

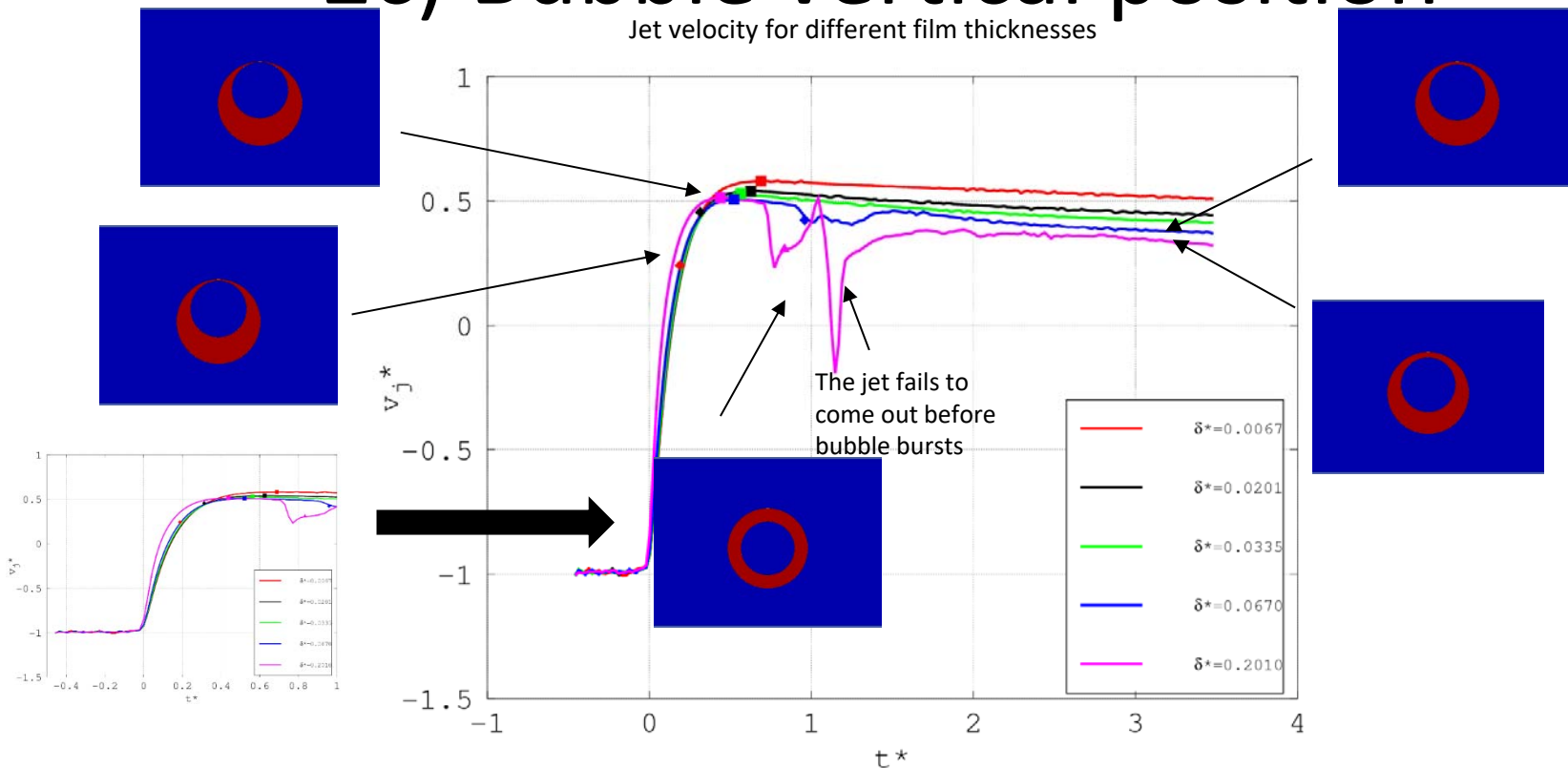


Axis pressure of  
different bubble sizes

● Burst time      ■ Maximum jet velocity time

# 2c) Bubble vertical position

Jet velocity for different film thicknesses

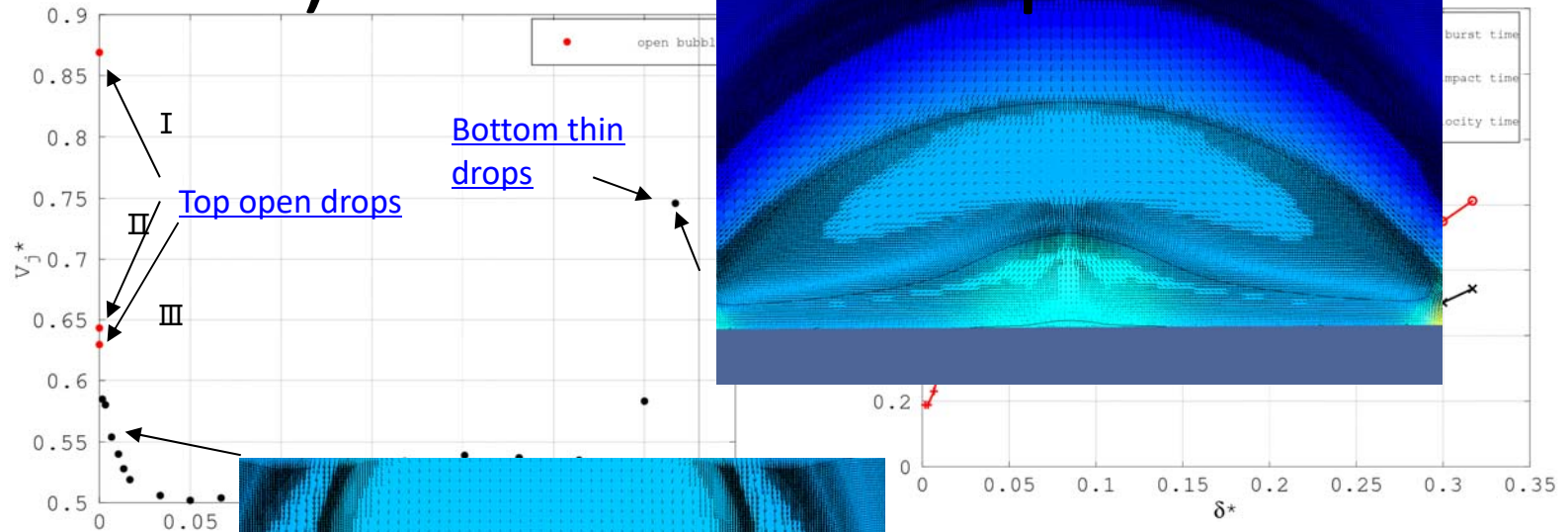


◆ Burst time   
 ▲ Jet impact   
 ■ Maximum jet velocity time

$V = 4.276\text{m/s}$ ,  $D_b^* = 0.67D$ ,  $\delta^* = 0.0067, 0.0210, 0.0335, 0.0670, 0.2010$ .

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# 2c) Bubble vertical position

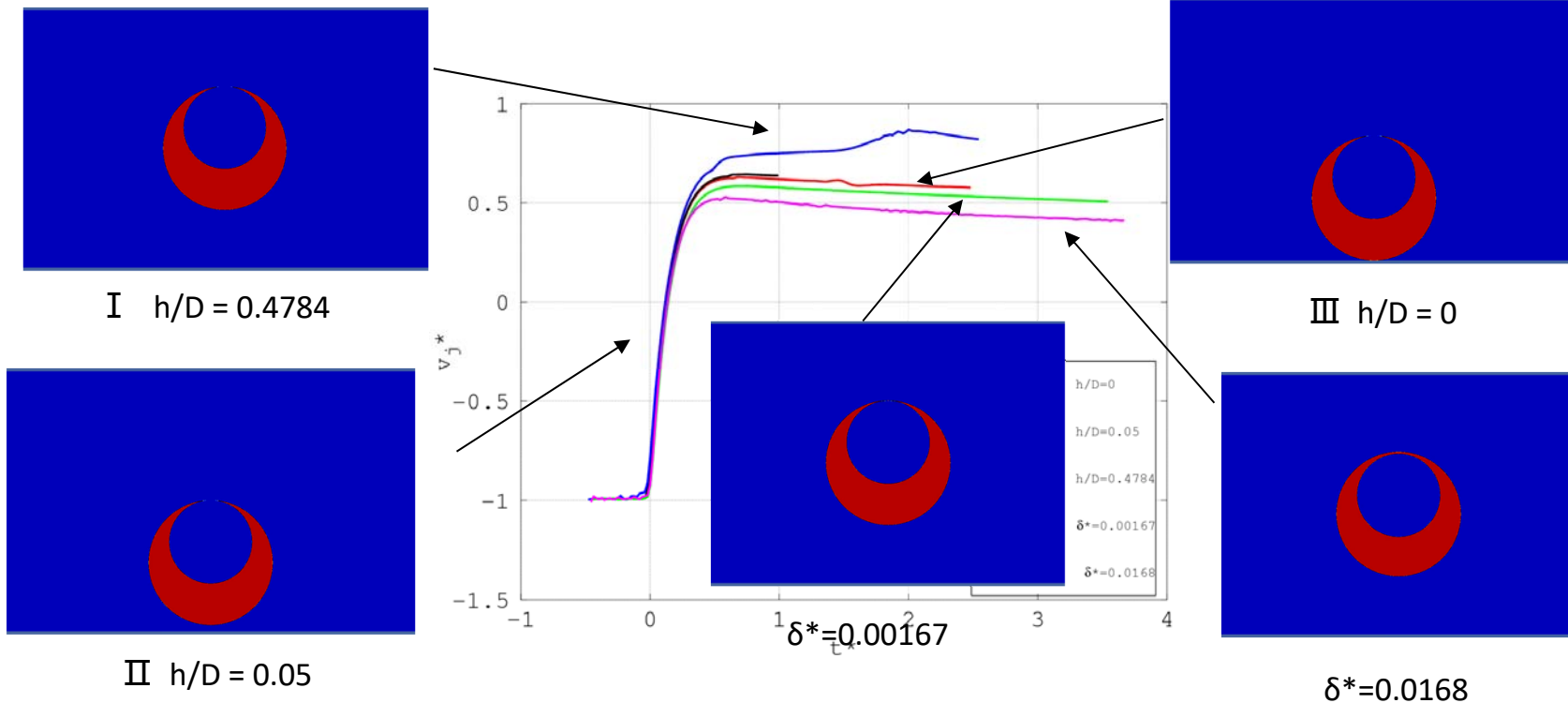


The relation  
 different film thickness  
 jet velocity decrease  
 But after  $\delta^* > 0.1$

Burst, impact and maximum jet velocity  
 time of different film thickness

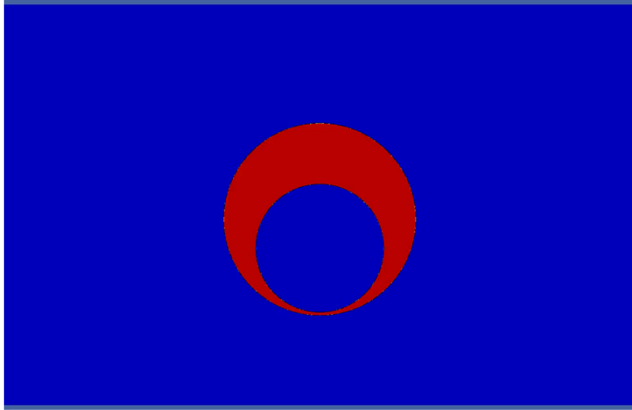
# Thin top film

Top open drops with different initial distances to the solid surface

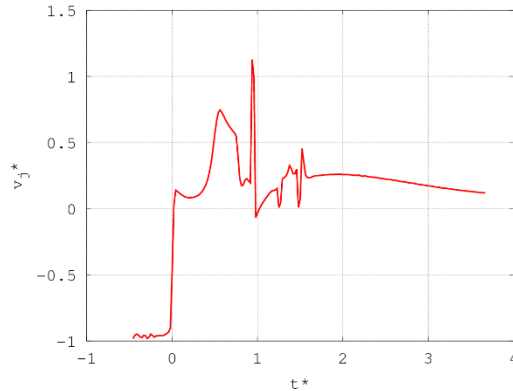
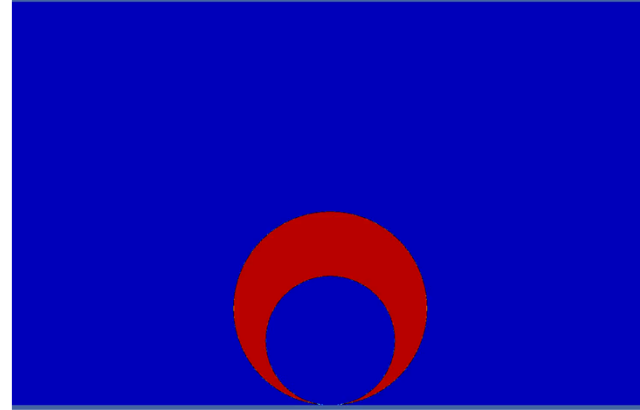


# Thin bottom film

Bottom thin drop

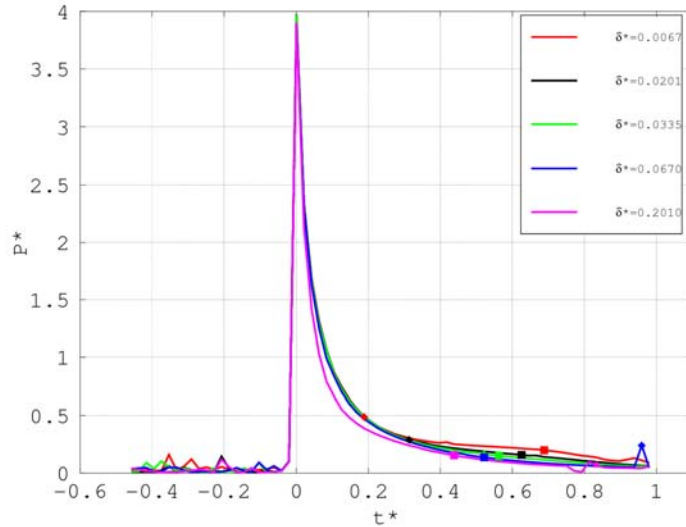


Bottom open drop

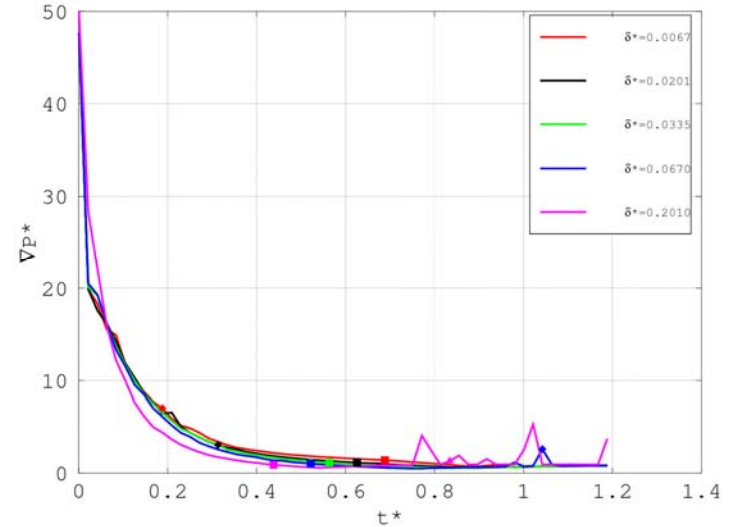


# 2c) Bubble vertical position

Maximum pressure on axis



Maximum vertical pressure gradient on axis



◆ Burst time

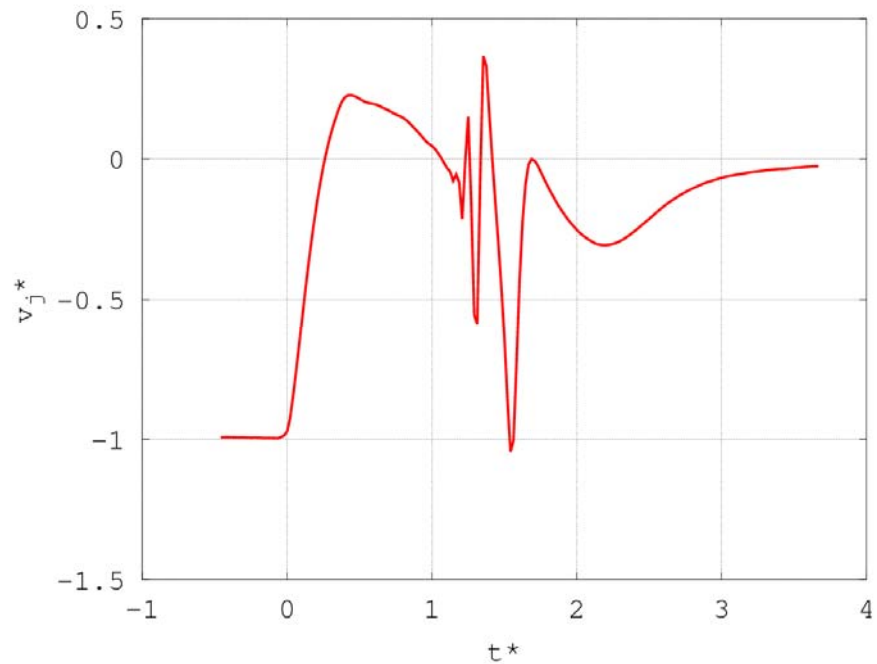
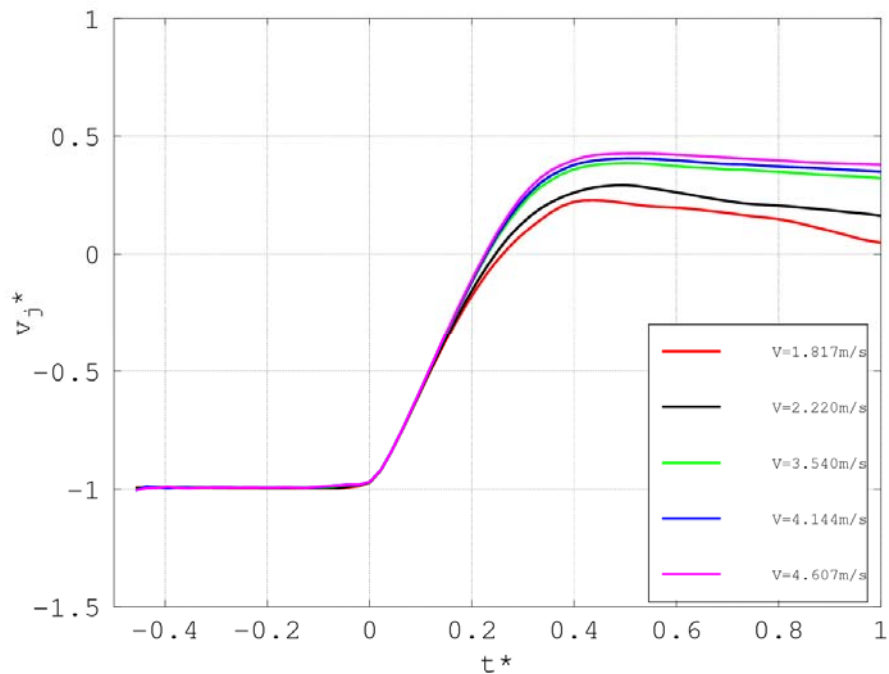
▲ Jet impact

■ Maximum jet velocity time

$V = 4.276\text{m/s}$ ,  $D_b^* = 0.67D$ ,  $\delta = 0.0067, 0.0210, 0.335, 0.0670, 0.2010$ .

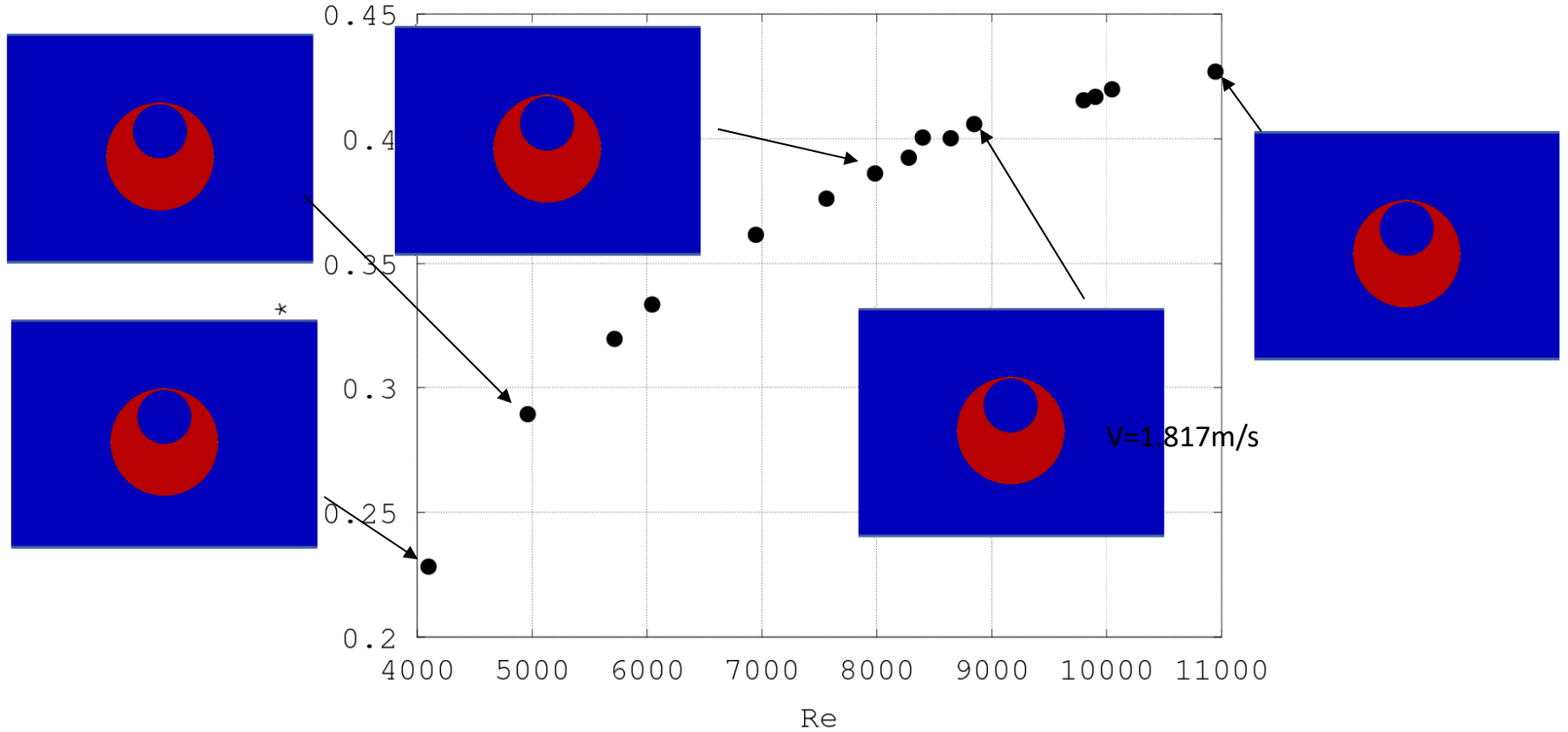
Different film thicknesses can also cause effect on non-dimensional pressure and non-dimensional pressure gradient. But the influence is not as significant as different bubble size.

# 2d) Liquid properties

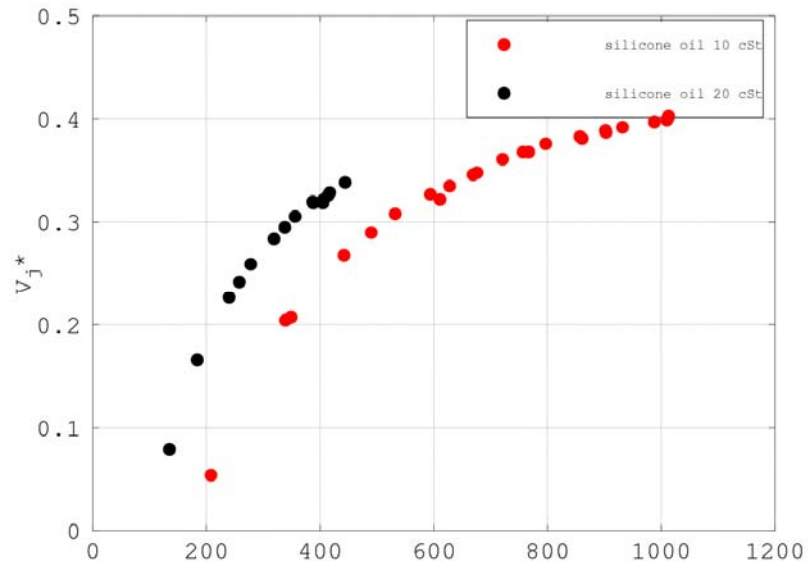




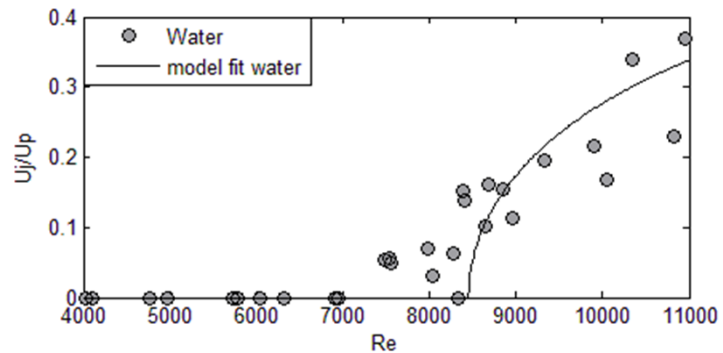
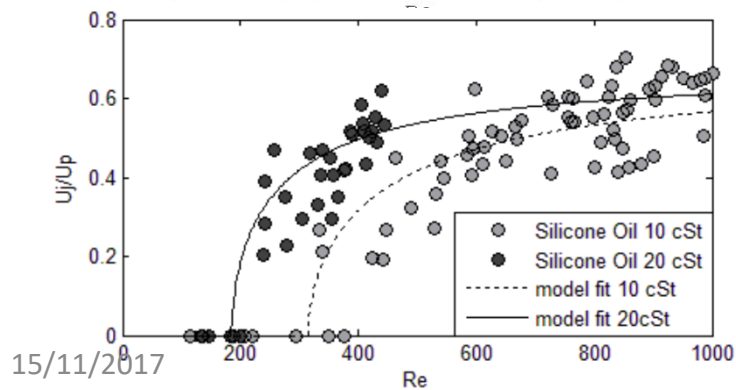
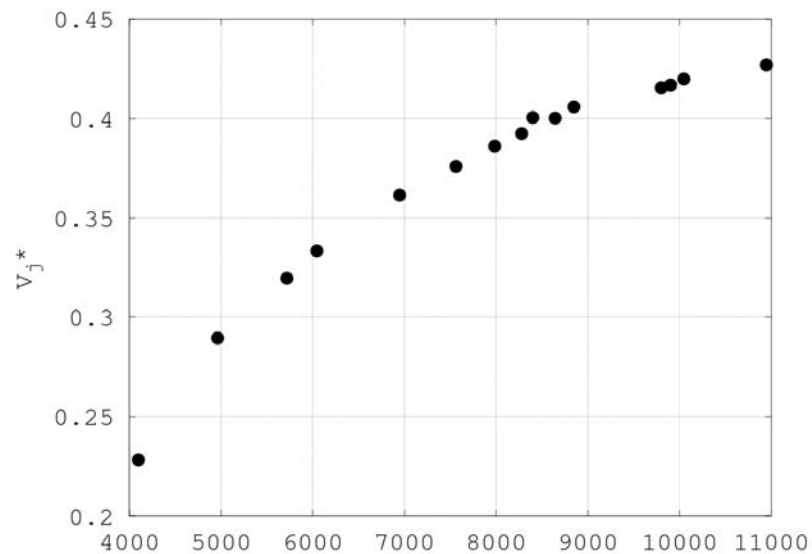
# 2d) Liquid properties

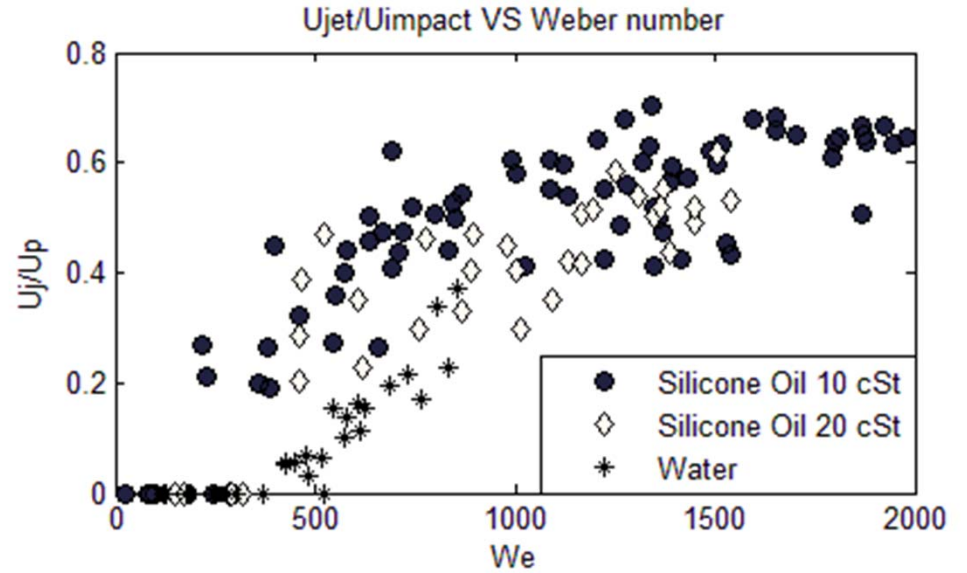
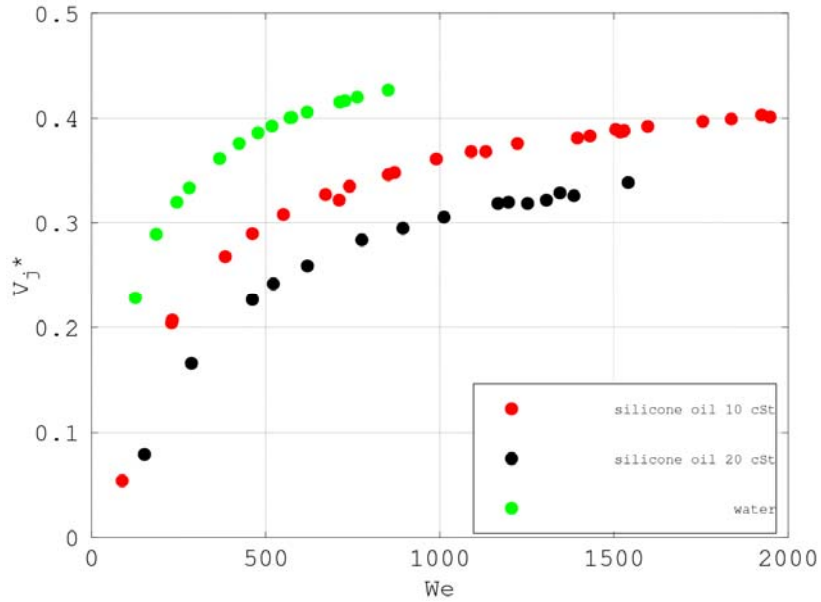


Silicone oil 10 cSt and 20 cSt



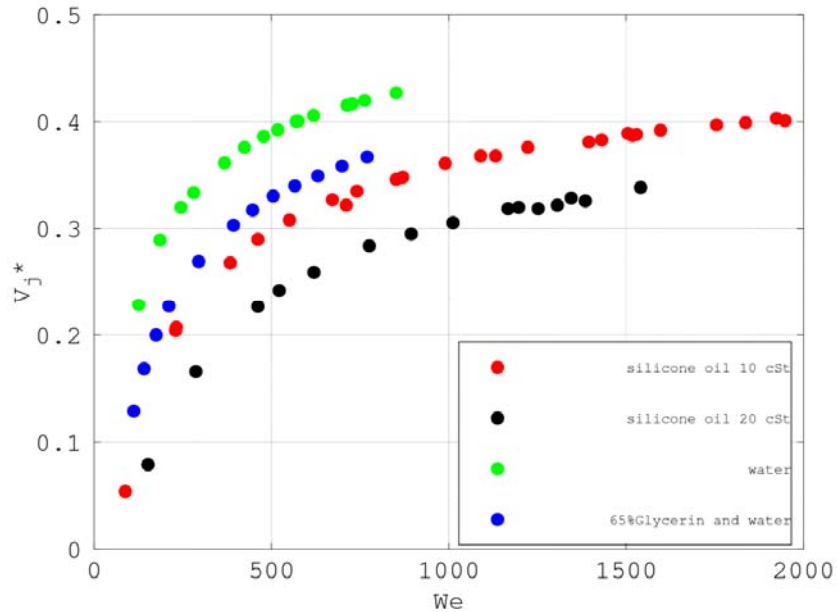
Water



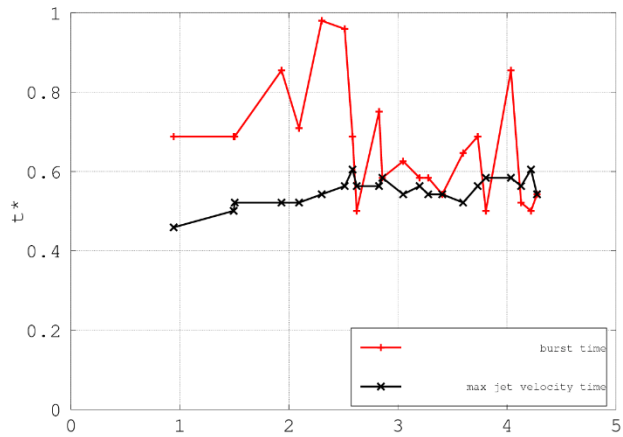


$V_j^*$  VS Weber number

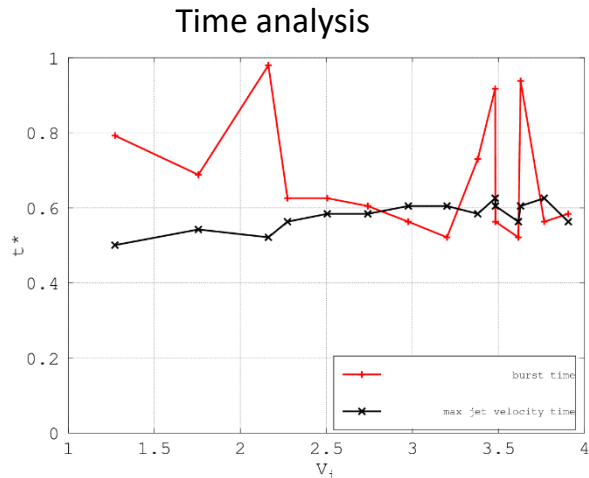
Water, silicone 10cSt, 20cSt and 65%glycerin  
with water



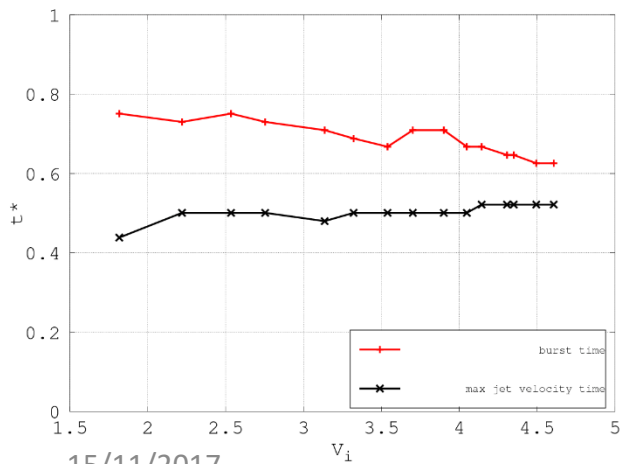
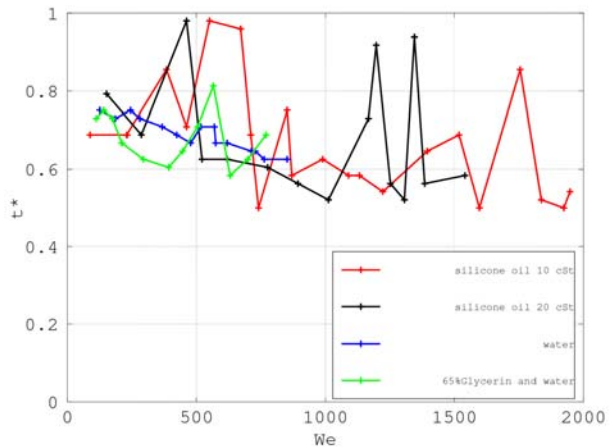
	Density(Kg/m <sup>3</sup> )	Surface tension (mn/m)	Viscosity(mPa·s)
Silicone oil 10 cSt	930	20.1	9.49
Silicone oil 20 cSt	950	20.8	18.49
water	997	72	1.216
65% glycerin with water	1165	66.7	12.2



Silicone oil 10 cSt

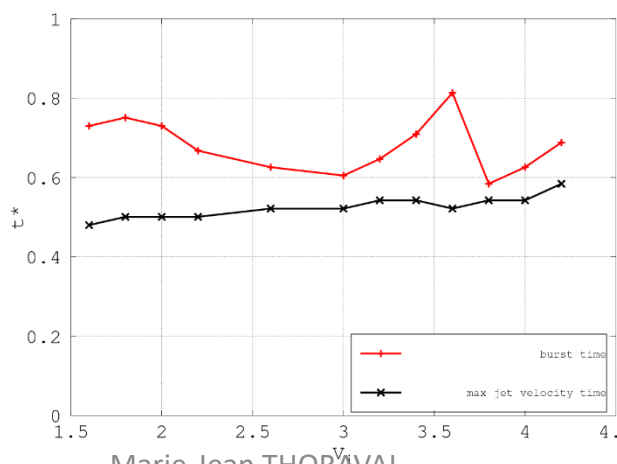


Silicone oil 20 cSt



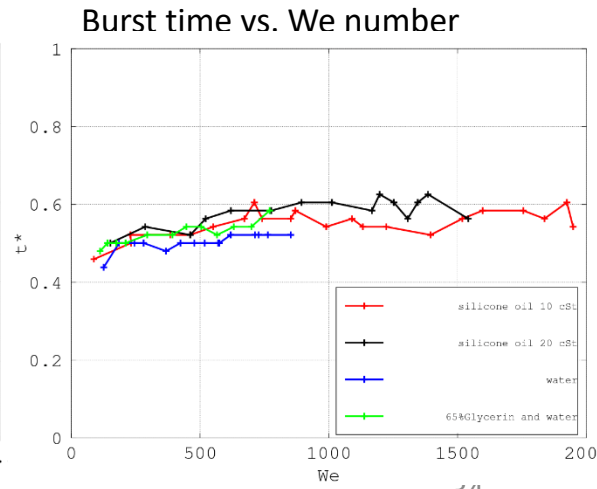
15/11/2017

water



Marie-Jean THORAVAL

65% glycerin with water



Maximum jet velocity time



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- Profs. Snoeijer & Lohse: University of Twente, **The Netherlands**



唐仲英基金会  
Cyrus Tang Foundation

# Super-fast jet!

$$V_j = 4.4!$$