

DNS of an Atomizing Biodiesel Jet with Basilisk

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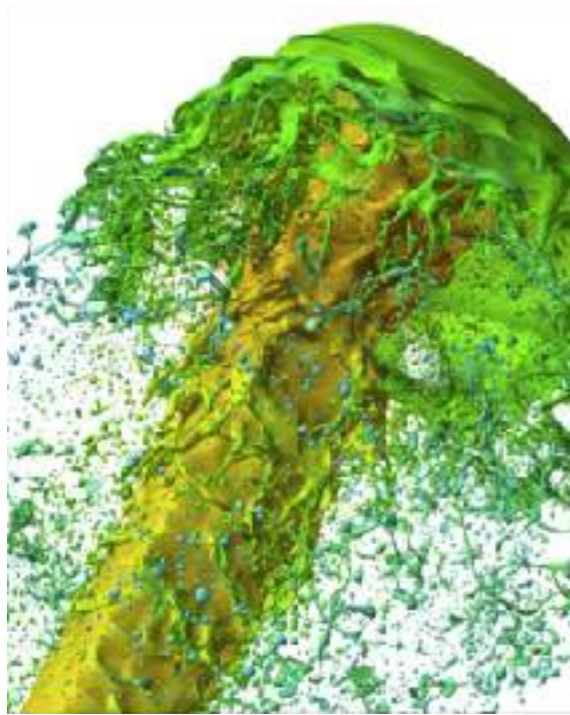
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Motivations

- ❖ Fuel injection and the resulting spray characteristics are critical to diesel engines
- ❖ Biodiesel fuels are increasingly popular
- ❖ Physical properties of biofuels have an impact on atomization process (*Pandey et al, 2012*)
- ❖ Direct Numerical simulations of atomization
 - ❖ Primary breakups
 - ❖ Turbulence-interface interaction
 - ❖ Droplets statistics

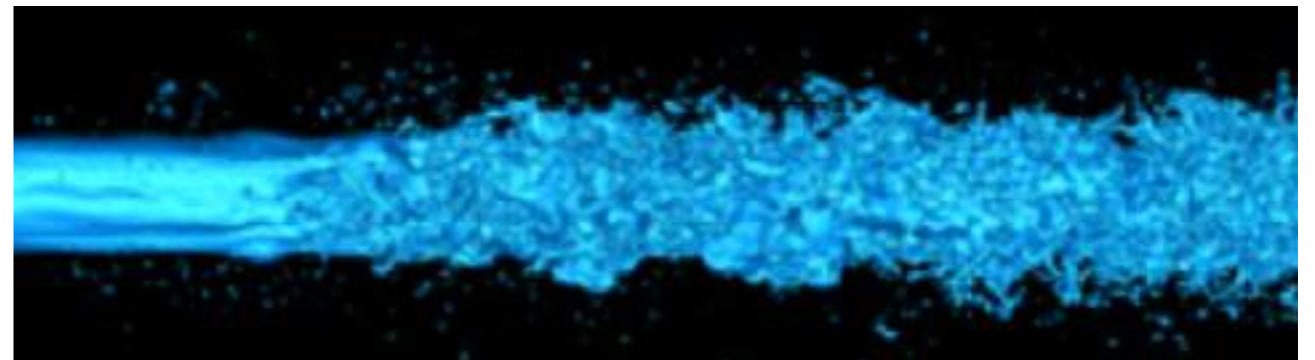
Detailed Numerical Simulation



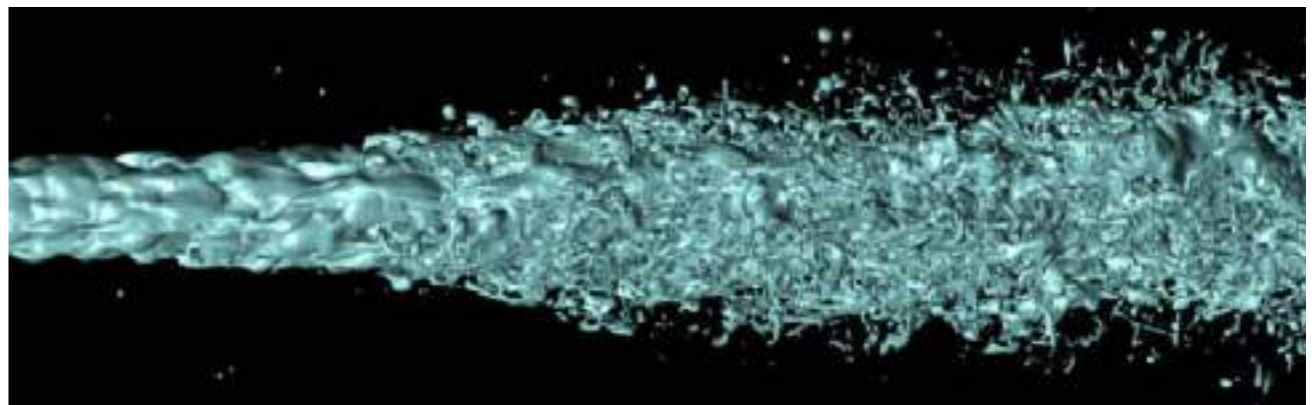
*Shinjo & Umemura
(2010)*



*Rana & Herrmann
(2011)*



Desjardins, Moureau & Pitsch (2008)



Lebas, Menard, Berlemont, et al. (2009)



Jarrahbashi, Sirignano, et al. (2016)



Le Chenadec & Pitsch (2013)

Equations & Solvers

- ❖ Incompressible variable-density, N-S equations with surface tension

$$\rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot (2\mu \mathbf{D}) + \sigma \kappa \delta_s \mathbf{n}$$
$$\nabla \cdot \mathbf{u} = 0$$

- ❖ Volume of fluid method (PLIC)

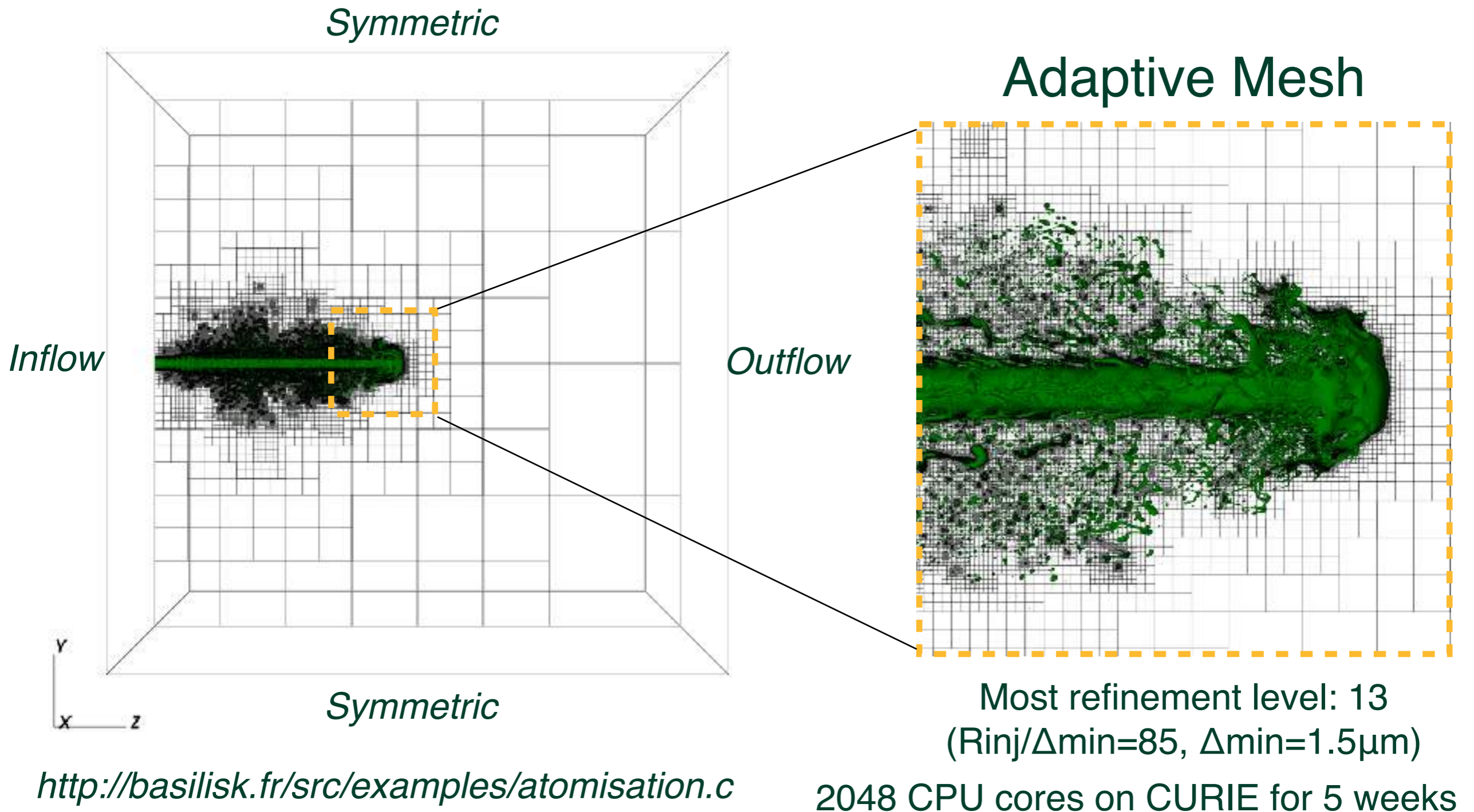
$$\partial_t C + \mathbf{u} \cdot \nabla C = 0$$

- ❖ Basilisk solver

Finite volume approach, 2nd order in time & space, VOF, quad/octree spatial discretization, adaptive mesh refinement, height-function method for curvature, balanced-force surface tension discretization



Simulation Setup



Simulation Cases

Gas: compressed air ($p=10$ bar)

Liquid fuels: - Standard European diesel (D)

- Biodiesel of soybean Methyl Ester (B)

Fuels	ρ_g (kg/m ³)	ρ_l (kg/m ³)	μ_g (Pa s)	μ_l (Pa s)	σ (N/m)
Diesel	11.13	825	1.46E-05	2.10E-03	2.4E-2
Biodiesel	11.13	870	1.46E-05	3.90E-03	2.8E-2

(Battistoni & Grimaldi, 2012, Appl. Energy, 97, pp. 656–666)

Three different injection conditions

Injection Cond.	R_{inj} (μm)	U_{inj} (m/s)
1	65	70
2	40	50
3	65	50

Simulation Cases

Cases	ρ_g (kg/m ³)	ρ_l (kg/m ³)	μ_g (Pa s)	μ_l (Pa s)	σ (N/m)	R_{inj} (μ m)	U_{inj} (m/s)	Re_g	Re_l	We_g	We_l
D1	11.13	825	1.46E-05	2.10E-03	2.4E-2	65	70	6940	3580	295	21900
D2	11.13	825	1.46E-05	2.10E-03	2.4E-2	40	50	3050	1570	927	6880
D3	11.13	825	1.46E-05	2.10E-03	2.4E-2	65	50	4950	2550	151	11200
B1	11.13	870	1.46E-05	3.90E-03	2.8E-2	65	70	6940	2030	253	19800
B2	11.13	870	1.46E-05	3.90E-03	2.8E-2	40	50	3050	892	79.5	6210
B3	11.13	870	1.46E-05	3.90E-03	2.8E-2	65	50	4950	1450	129	10100

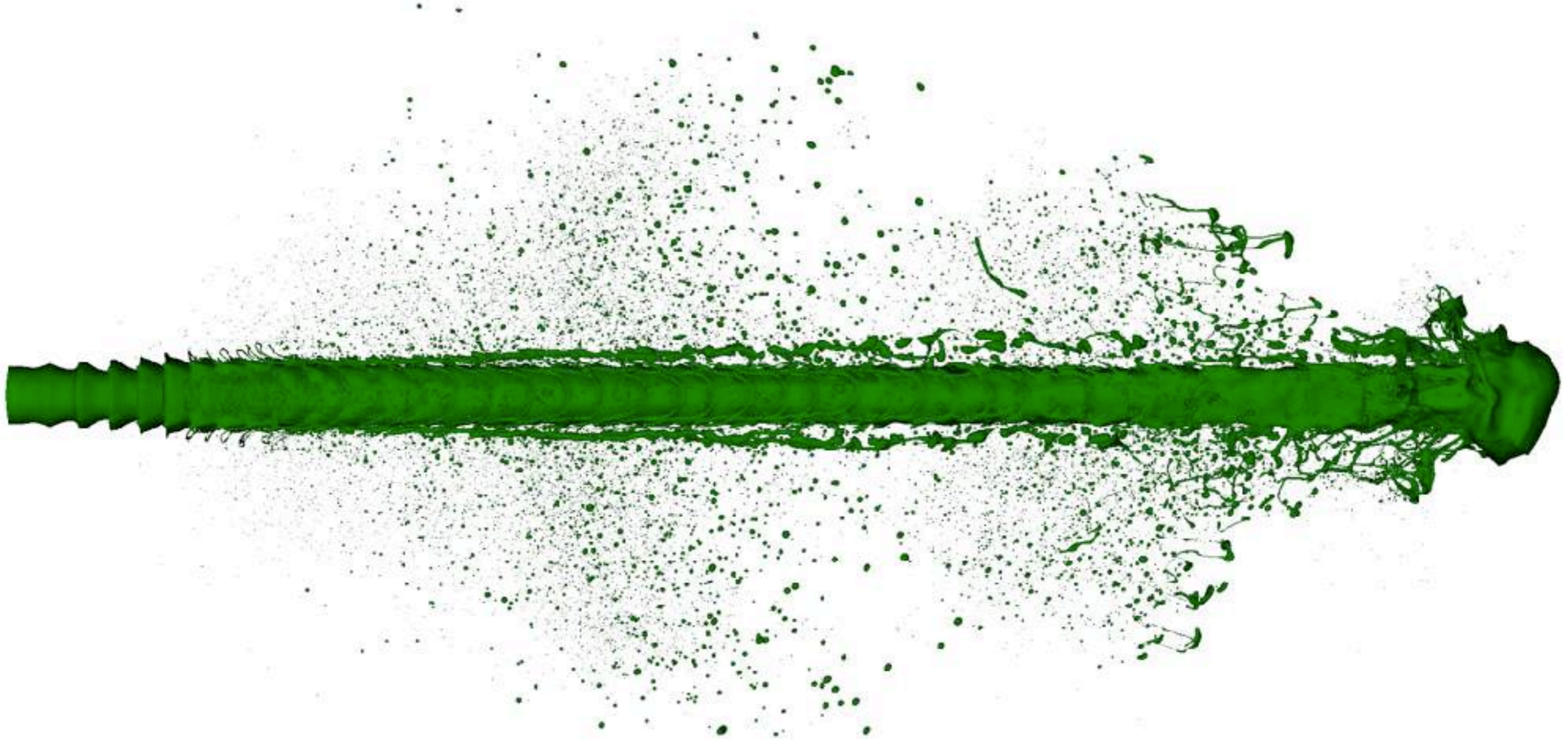
Gas: compressed air (p=10 bar)

Liquid fuels: - Standard European diesel (D1,D2, D3)

- Biodiesel of soybean Methyl Ester (B1, B2, B3)

1,2,3: three different injection conditions

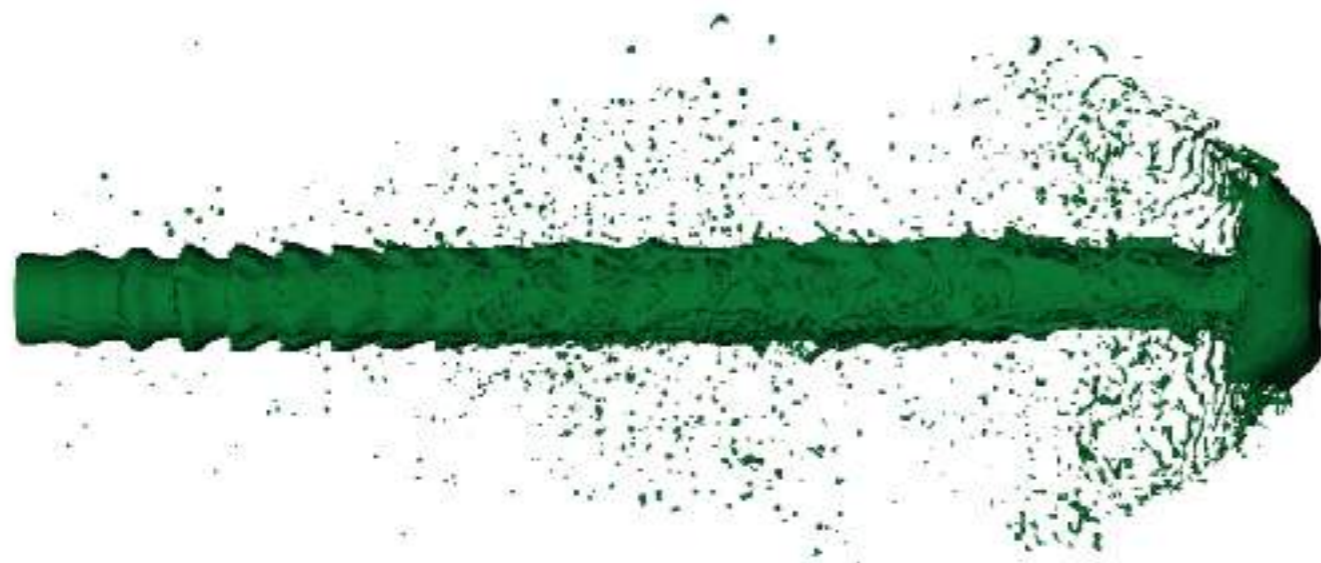
Atomizing Liquid Jet



Case B3, $R_{inj}/\Delta_{min}=85$
2048 Cores, about 3 weeks

Cases	Re_g	Re_l	We_g	We_l
B3	4950	1450	129	10100

Effect of Grid Resolution (B3)



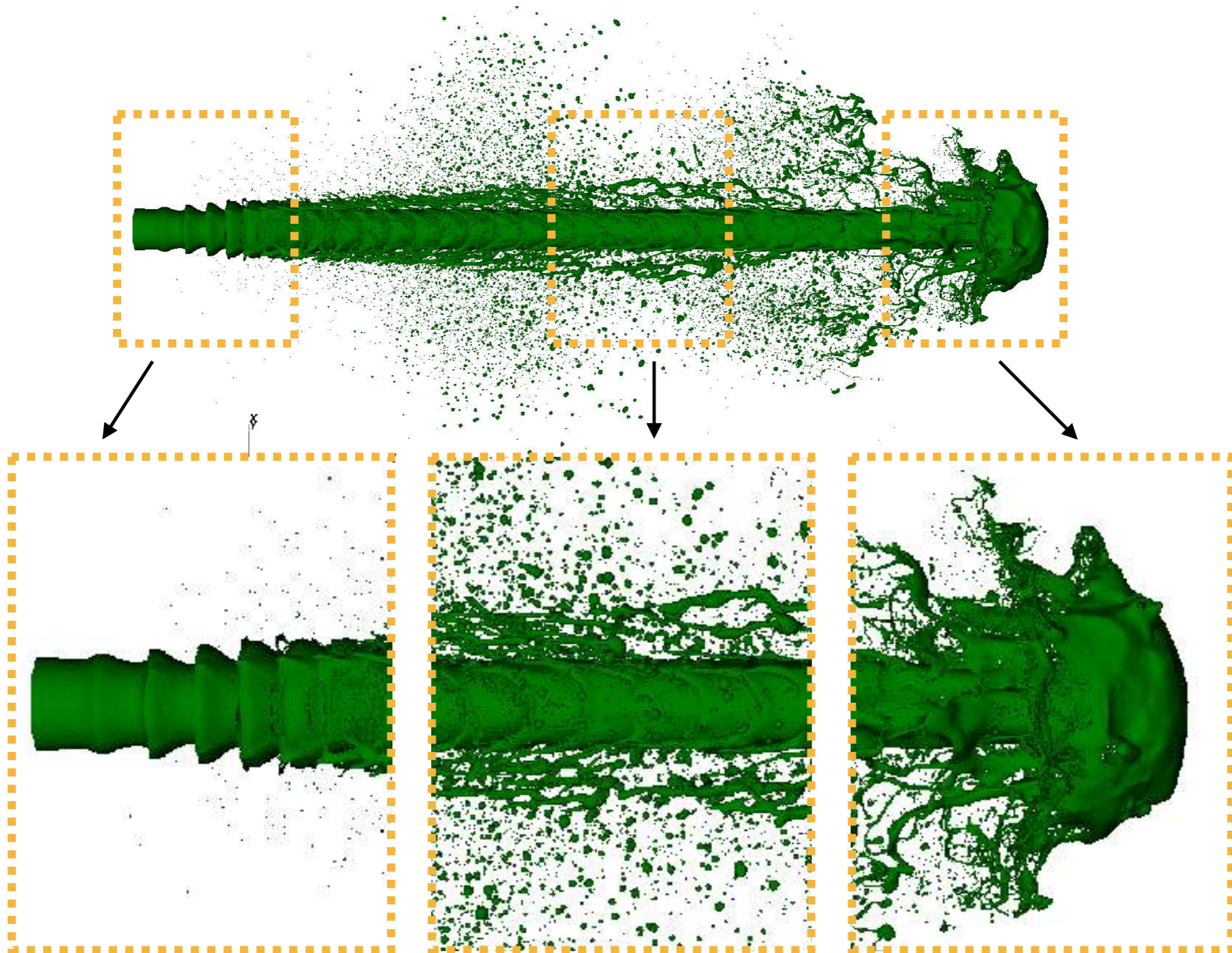
(a) $R_{inj}/\Delta_{min}=21$

(b) $R_{inj}/\Delta_{min}=43$

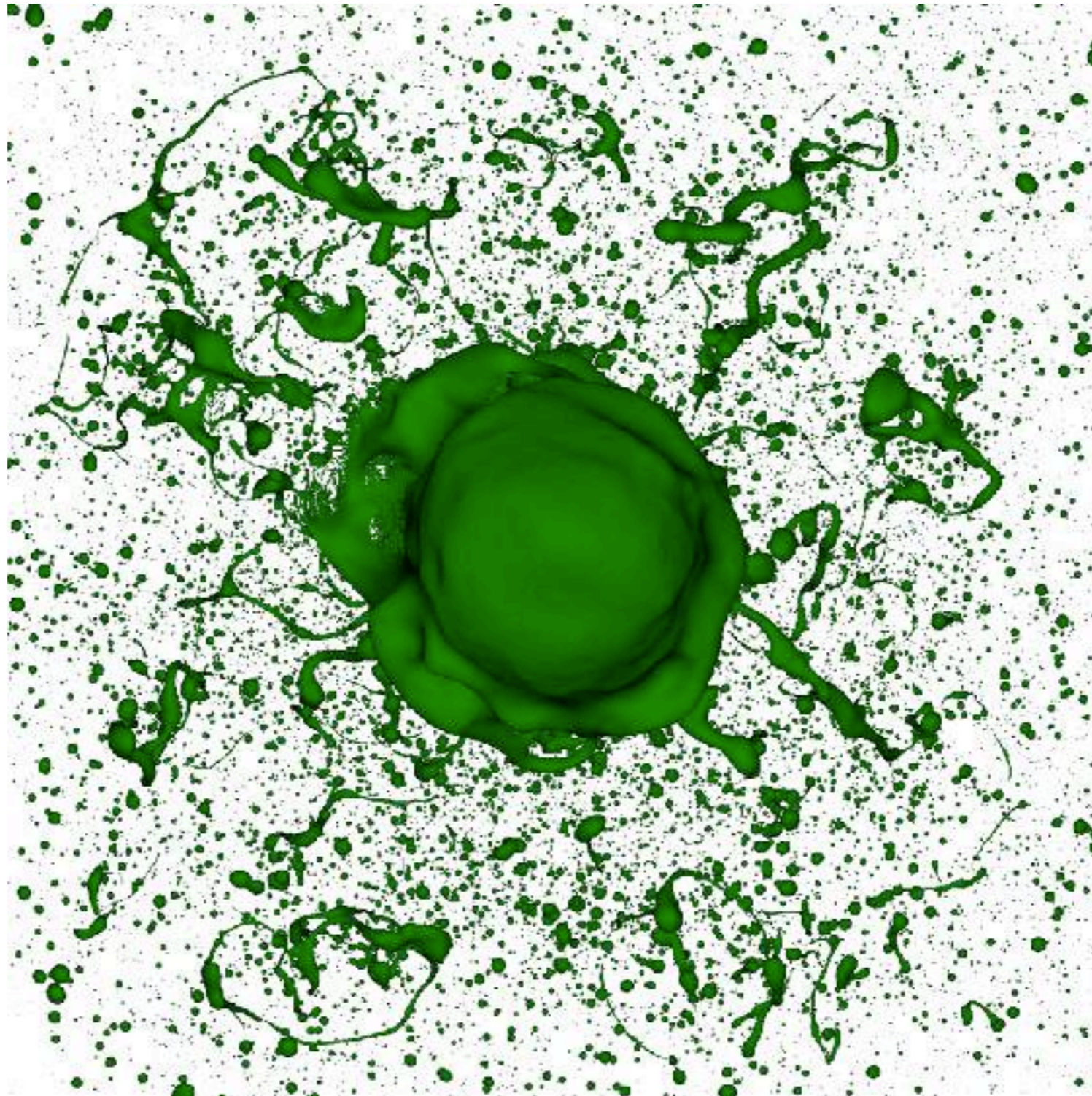


(c) $R_{inj}/\Delta_{min}=85$

Spray Formation

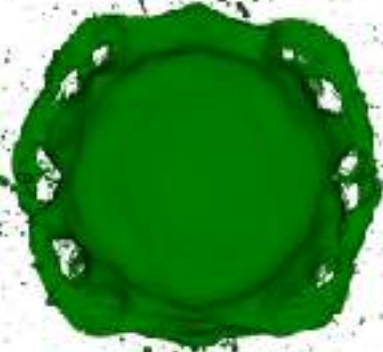


Dynamics of Mushroom Head



Dynamics of Mushroom Head

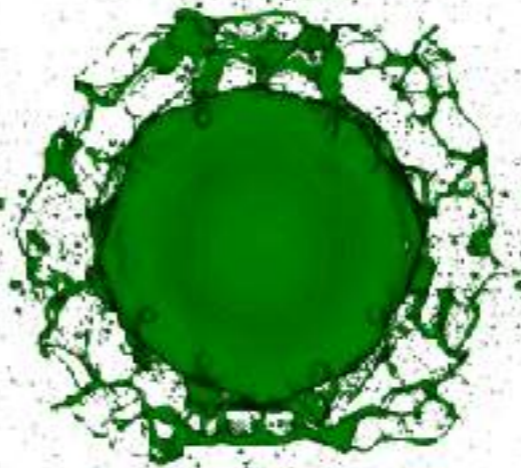
Hole formation



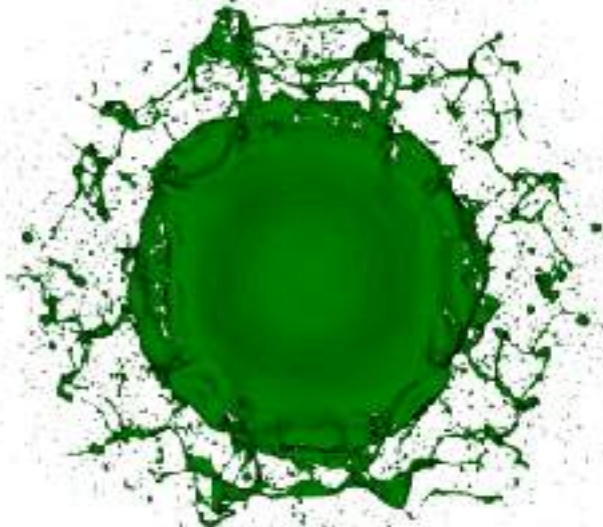
Hole Expansion



Ligaments



Droplets

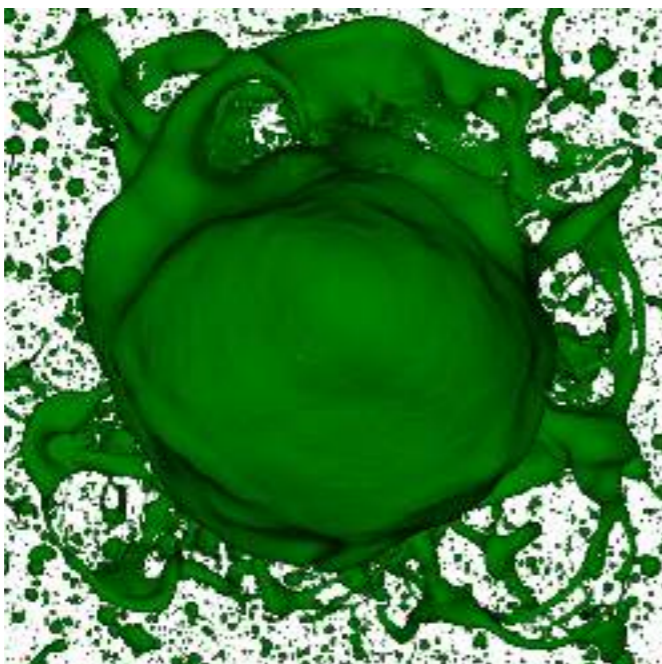
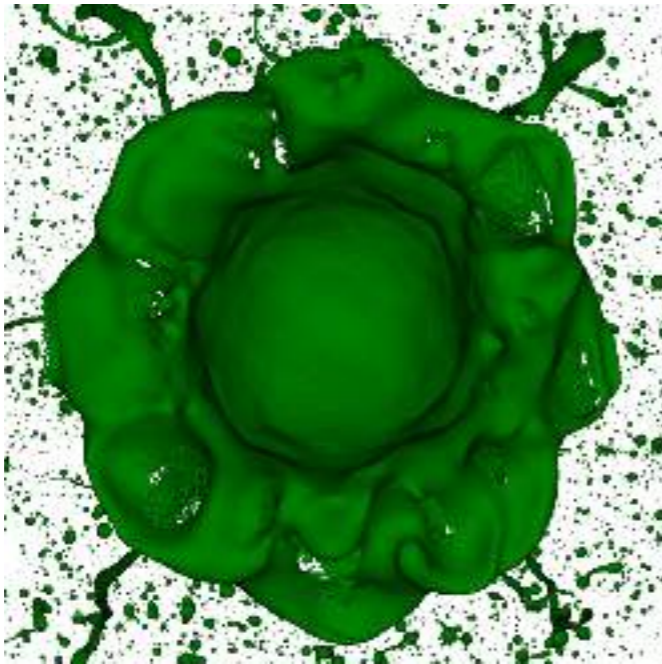


→ Time

Instability on the Head

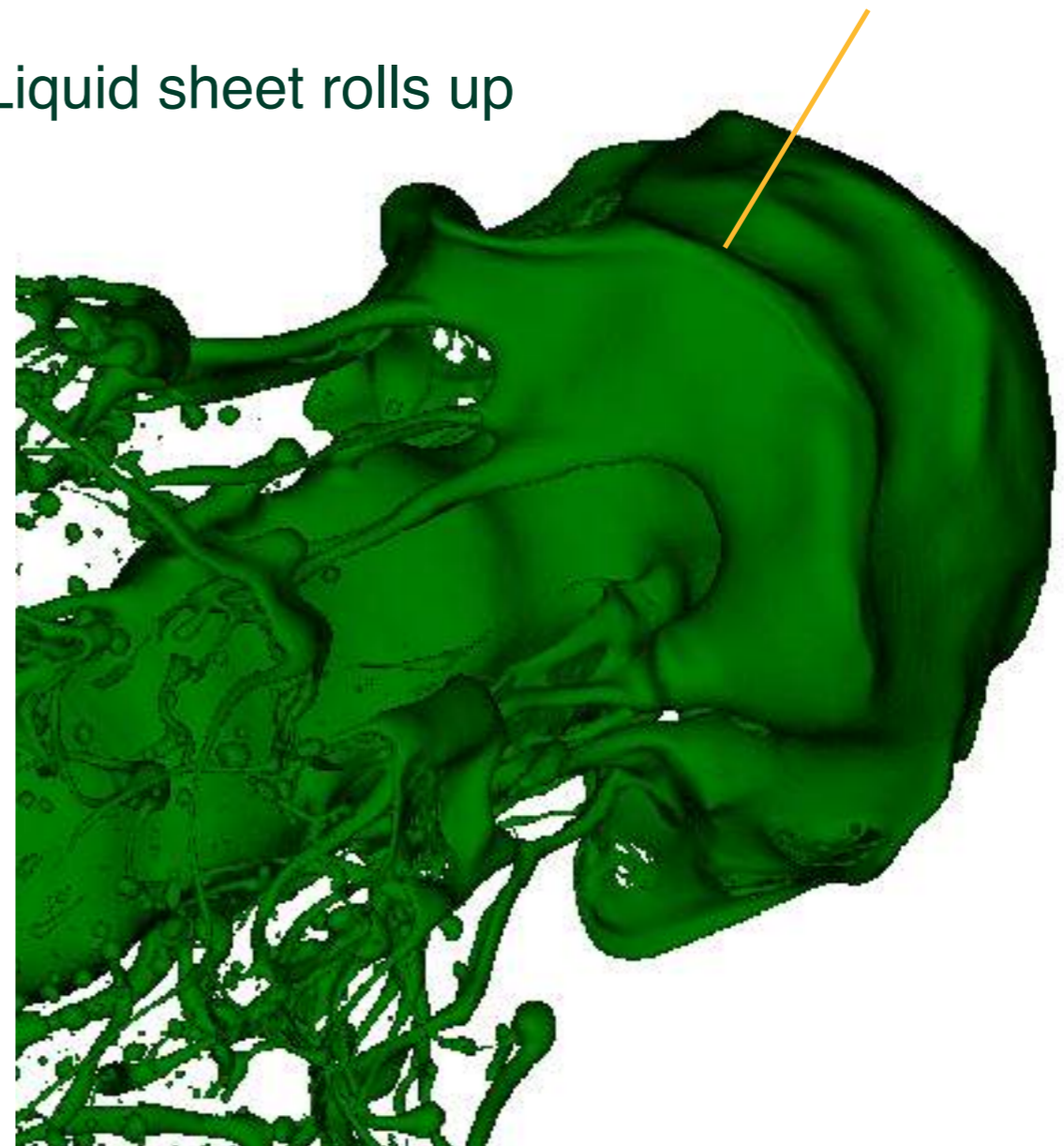
(Shinjo & Umemura 2010)

Helmholtz-Kelvin Instability



Time

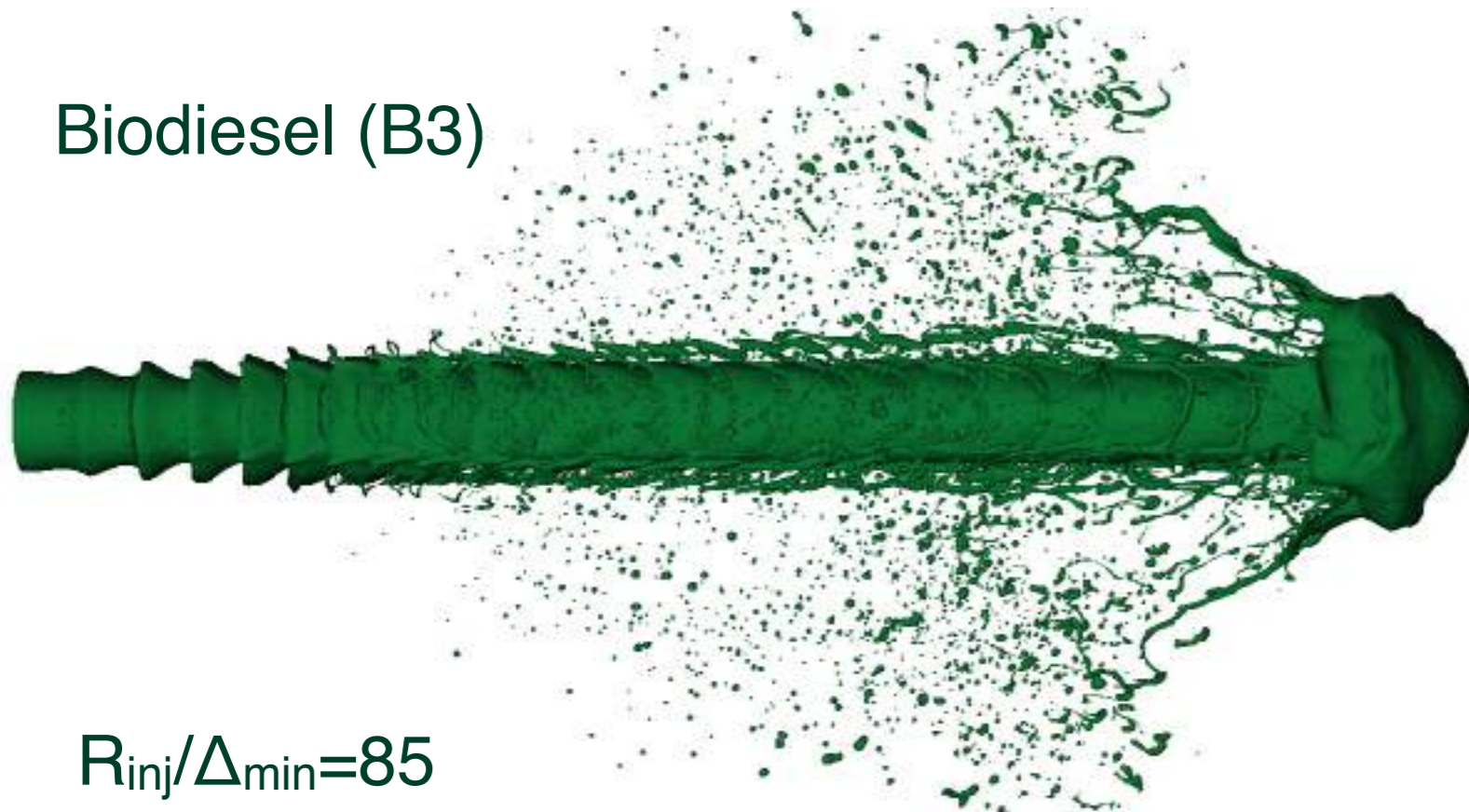
Liquid sheet rolls up



Effect of Cartesian grid fades out

Biodiesel vs Diesel

Biodiesel (B3)



- ❖ Longer filaments
- ❖ Smaller head
- ❖ Less droplets
- ❖ More large drops

$$R_{inj}/\Delta_{min}=85$$

Same injection conditions:

$$R_{inj}=65\mu\text{m}, U_{inj}=50\text{m/s}$$



Diesel (D3)

Cases	ρ_l (kg/m ³)	μ_l (Pa s)	σ (N/m)
D3	825	2.10E-03	2.4E-2
B3	870	3.90E-03	2.8E-2

Biodiesel vs Diesel: More Details

Biodiesel (B3)

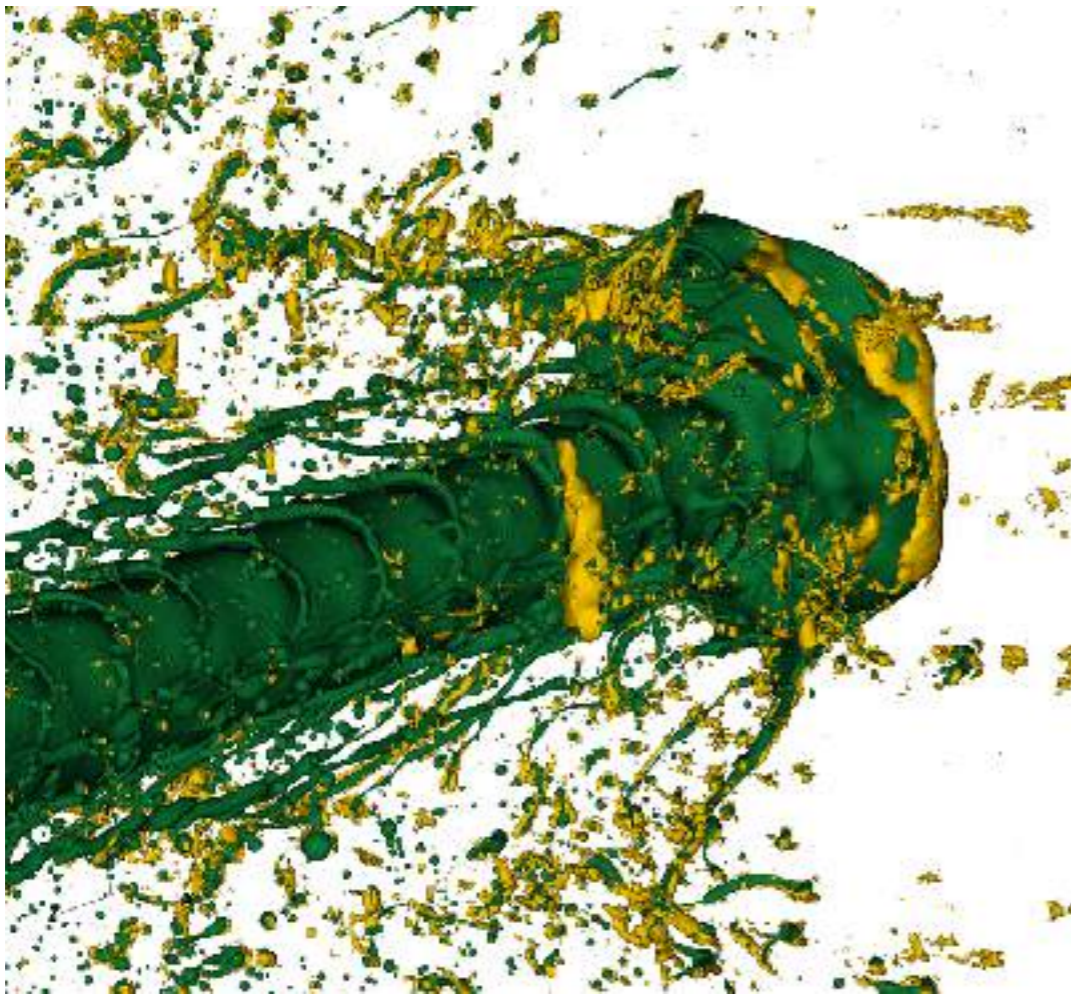


Diesel (D3)



Biodiesel vs Diesel: Vortices

λ_2 iso-surface for vortical structures visualization



Biodiesel (B3)



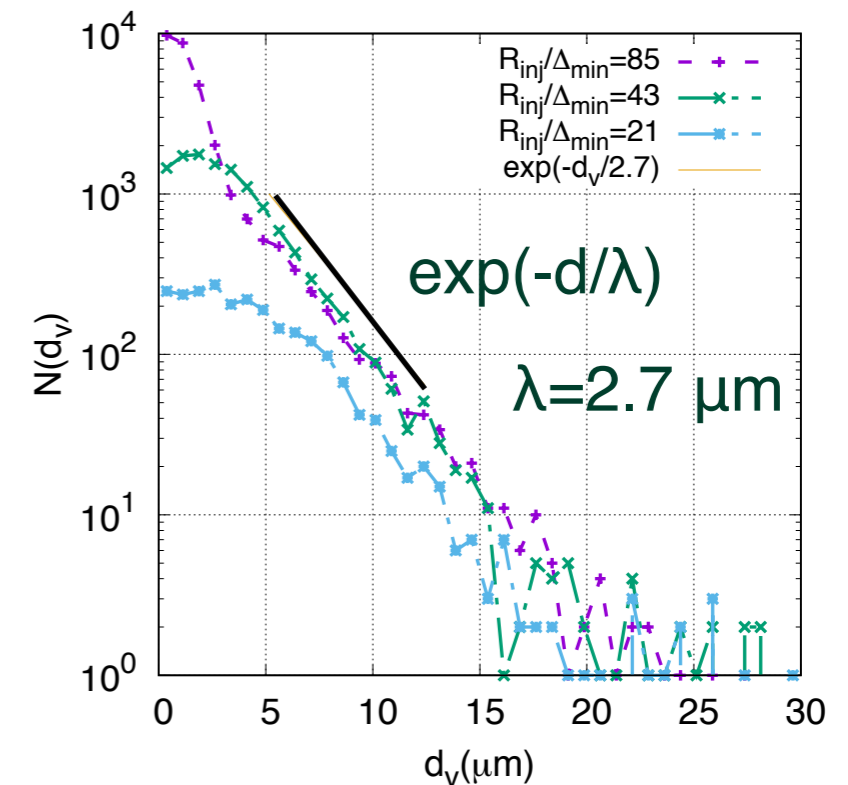
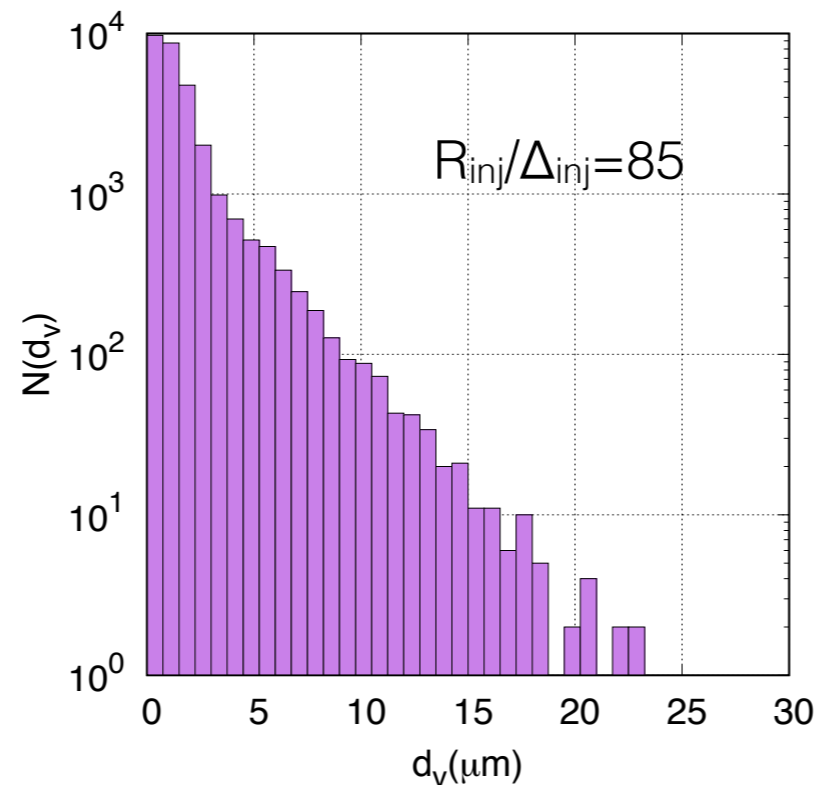
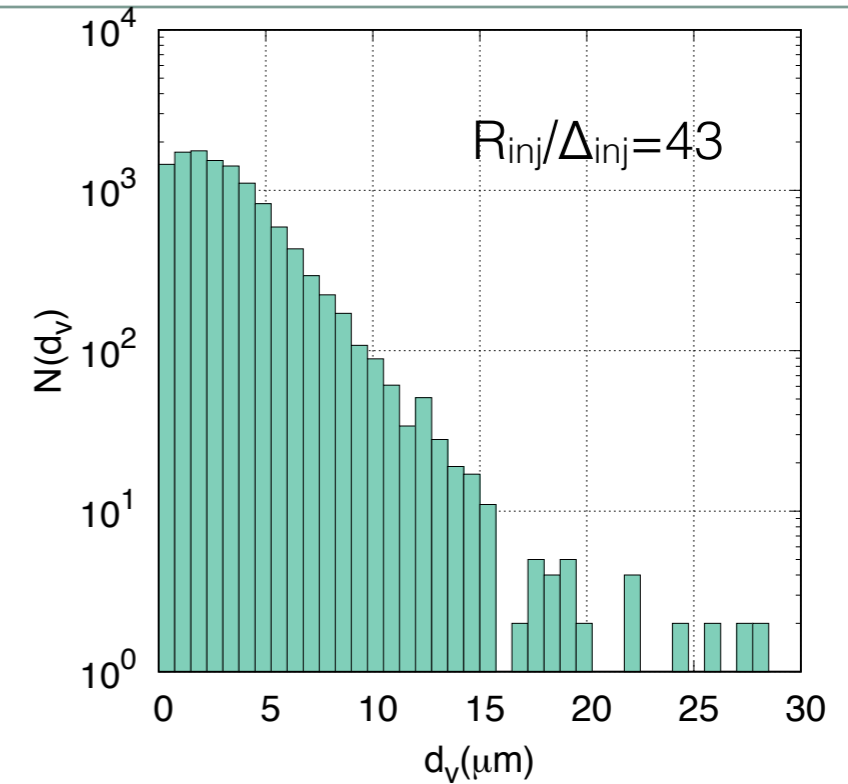
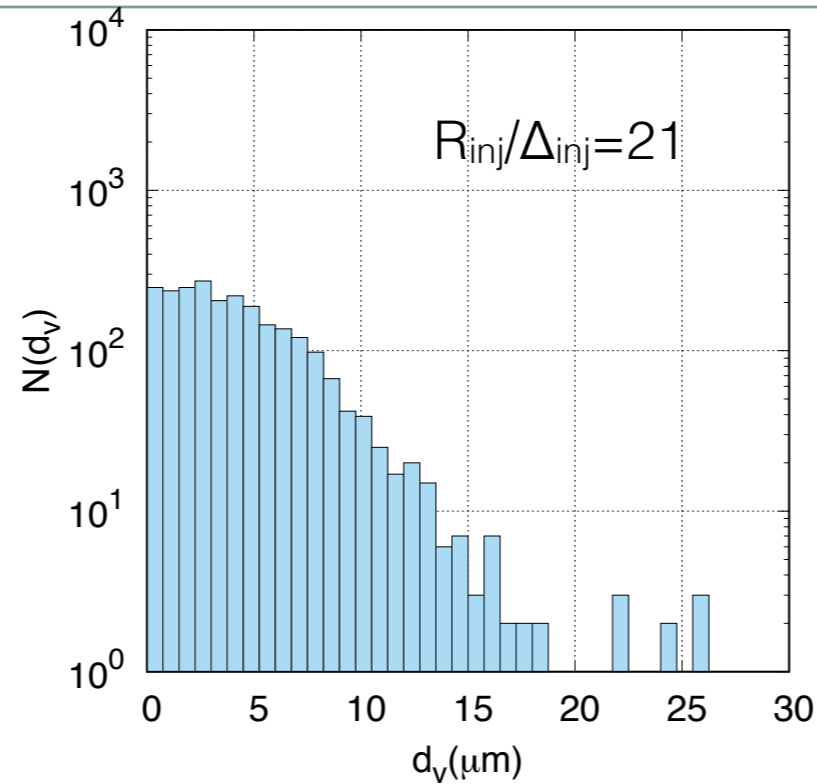
Diesel (D3)

(Vortex dynamics: Jarrahbashi, Sirignano, Popov, & Hussain 2016)

Droplet Size Distribution

Effect of grid resolution

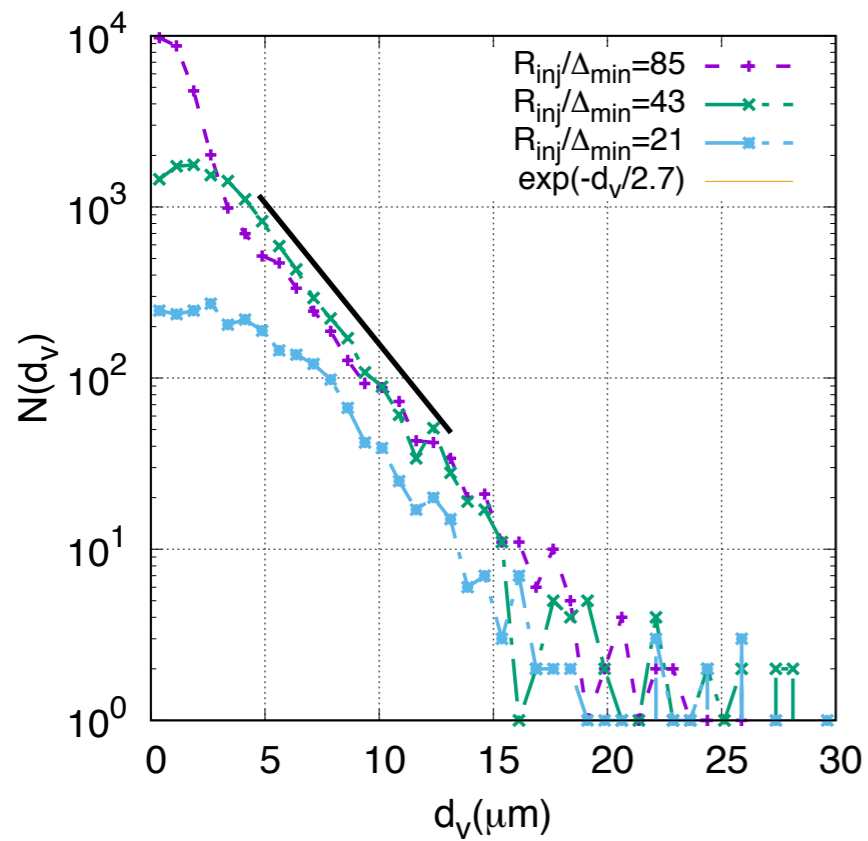
Biodiesel (B3)



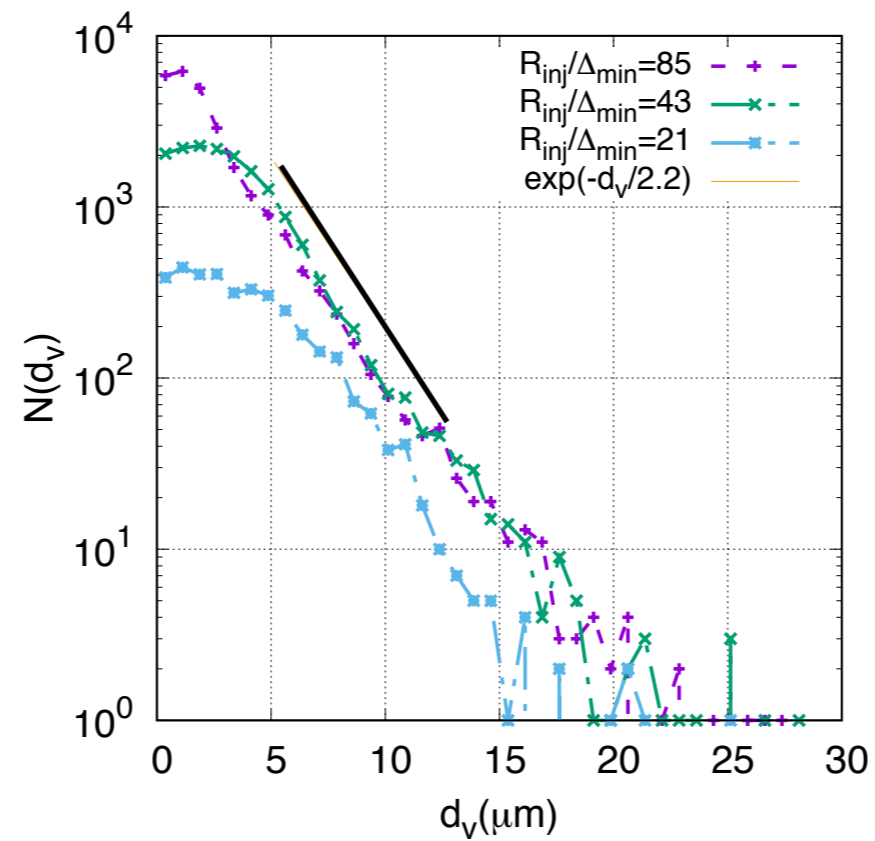
Marmottant & Villermaux
2004

Droplet Size Distribution

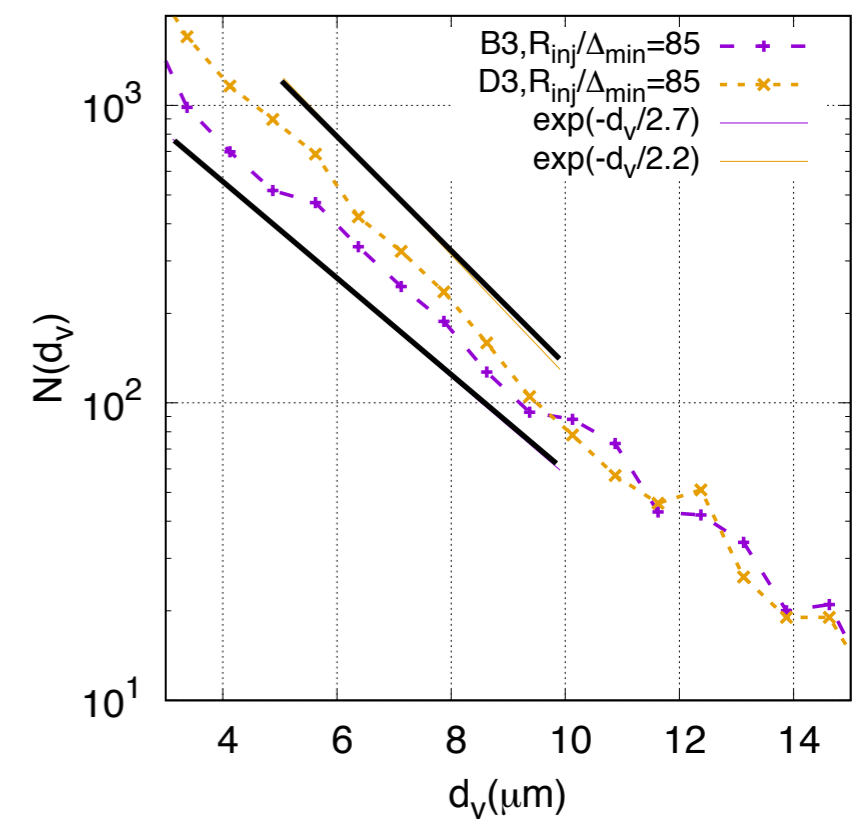
Biodiesel vs Diesel



Biodiesel (B3)



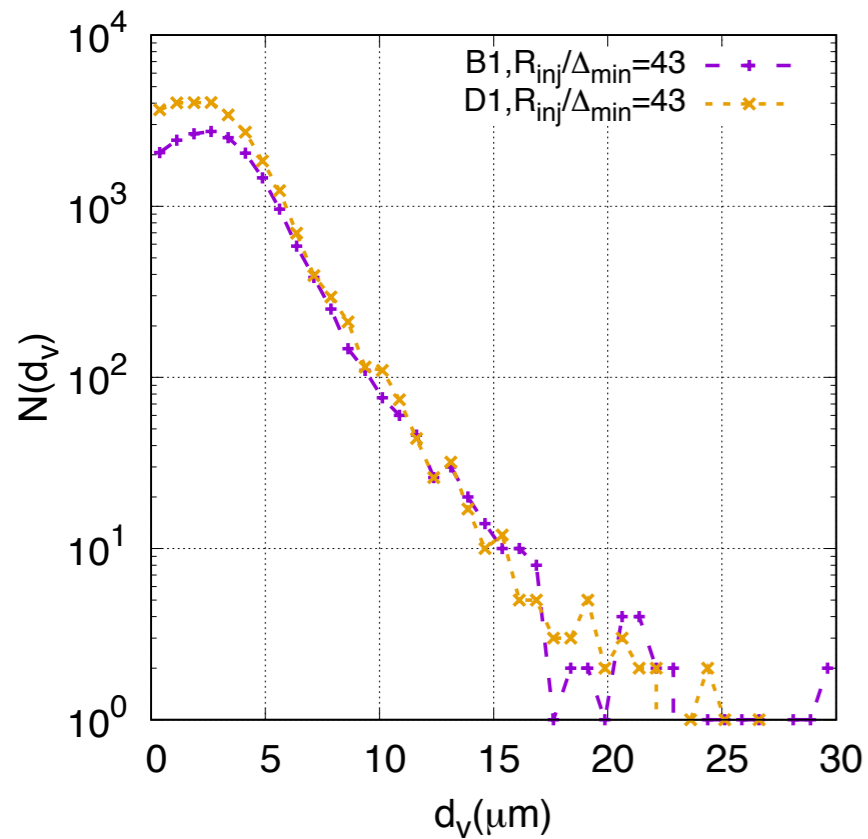
Diesel (D3)



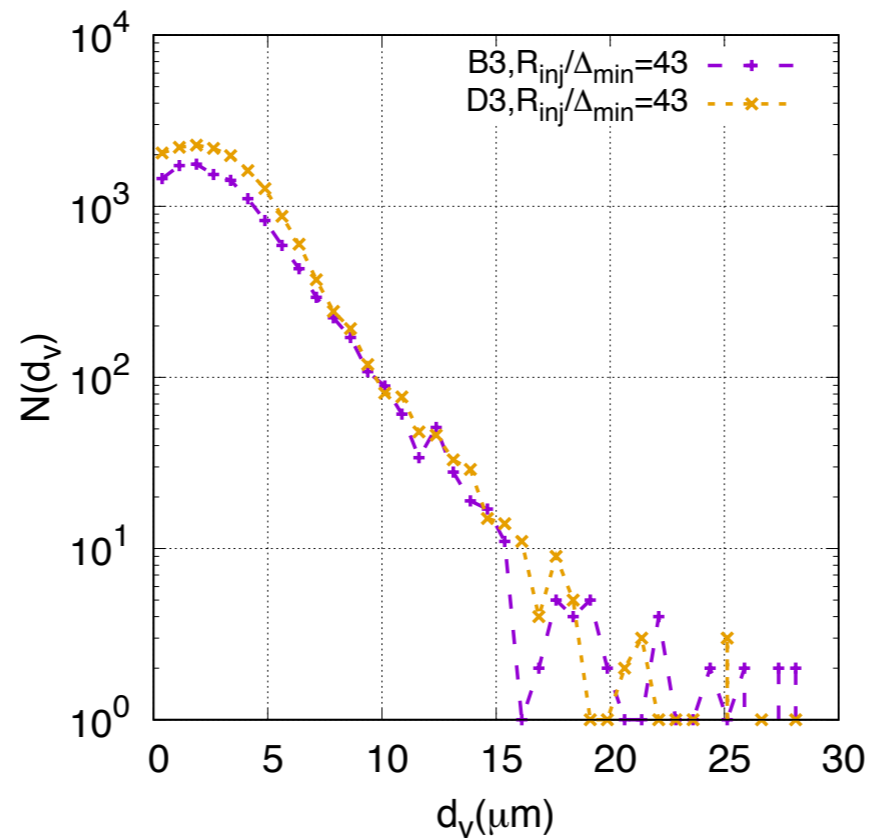
B3 vs D3

Droplet Size Distribution

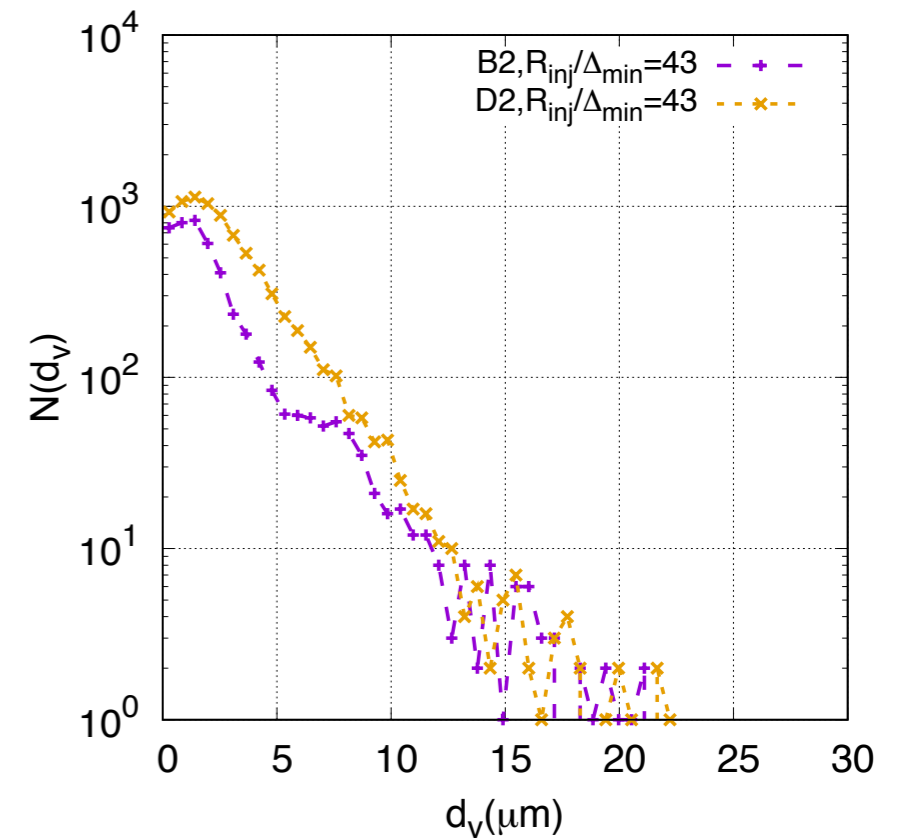
Effects of injection conditions



$R_{inj}=65\mu\text{m}$, $U_{inj}=70\text{m/s}$

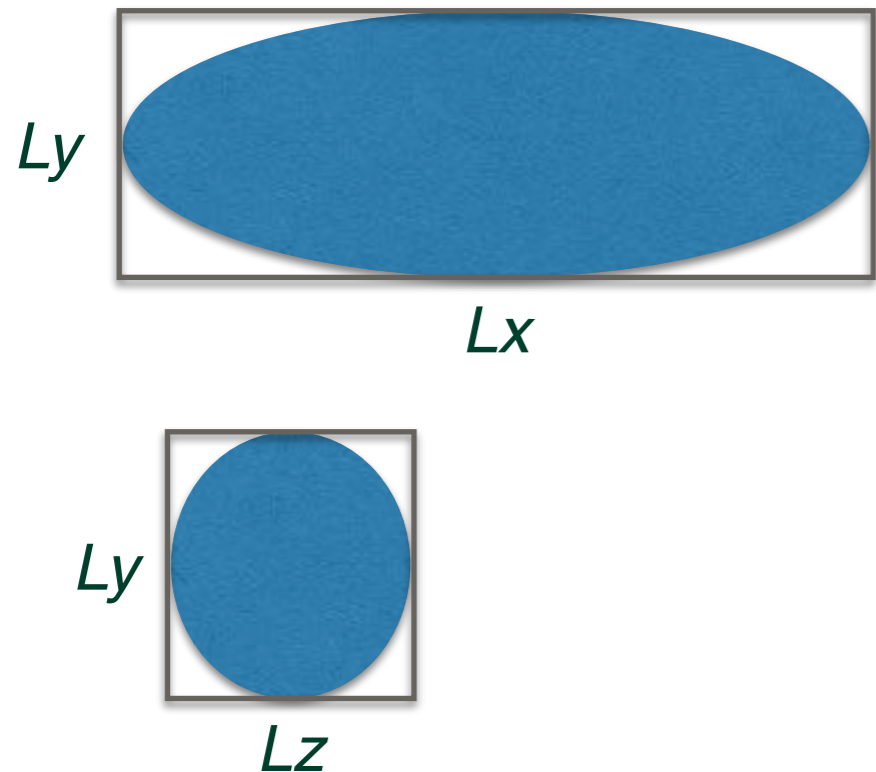


$R_{inj}=65\mu\text{m}$, $U_{inj}=50\text{m/s}$



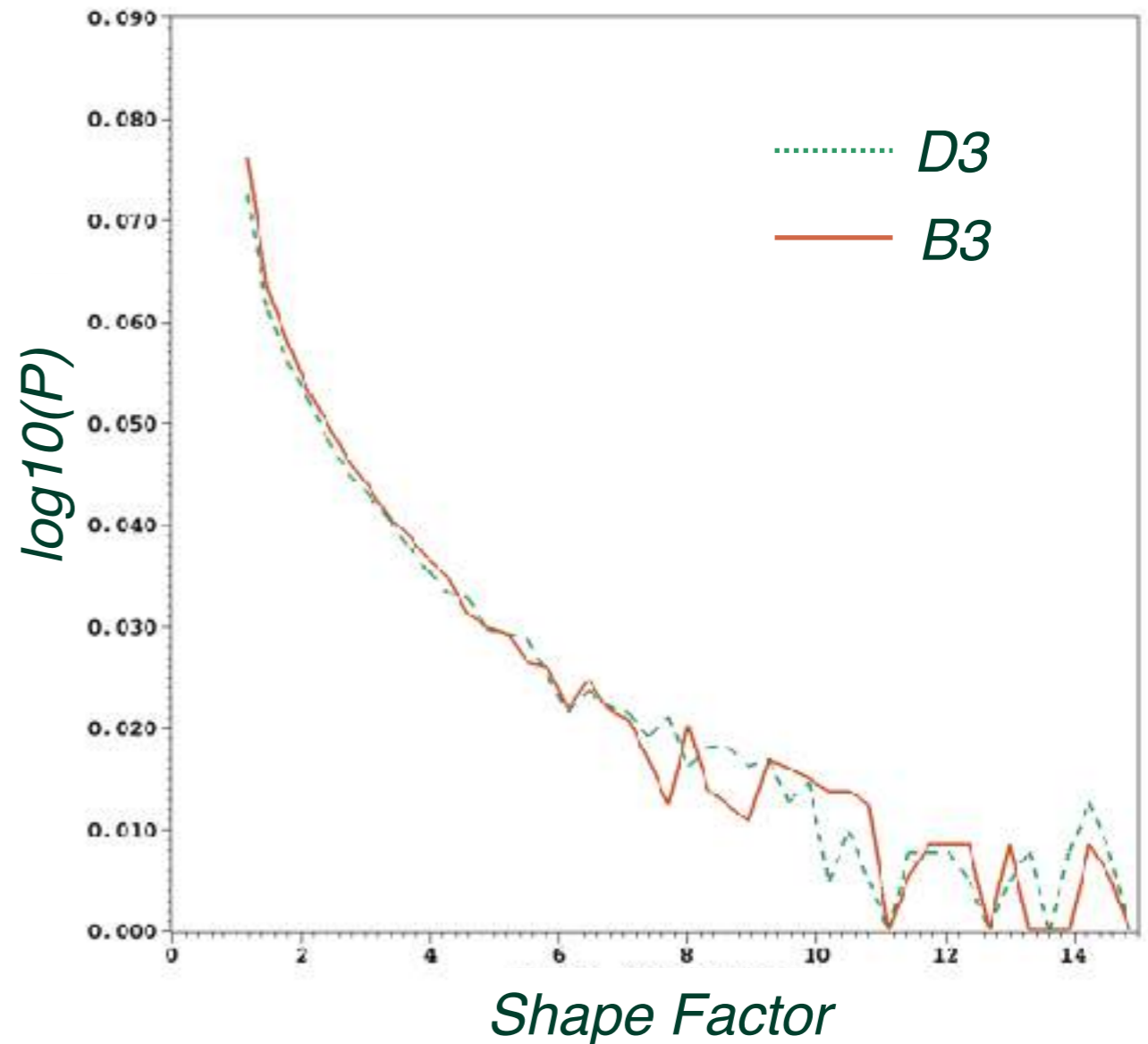
$R_{inj}=40\mu\text{m}$, $U_{inj}=50\text{m/s}$

Droplet Shape Characterization



Shape Factor = $\max(Lx, Ly, Lz) / \min(Lx, Ly, Lz)$

Occupancy Factor = $\text{Volume} / (Lx * Ly * Lz)$



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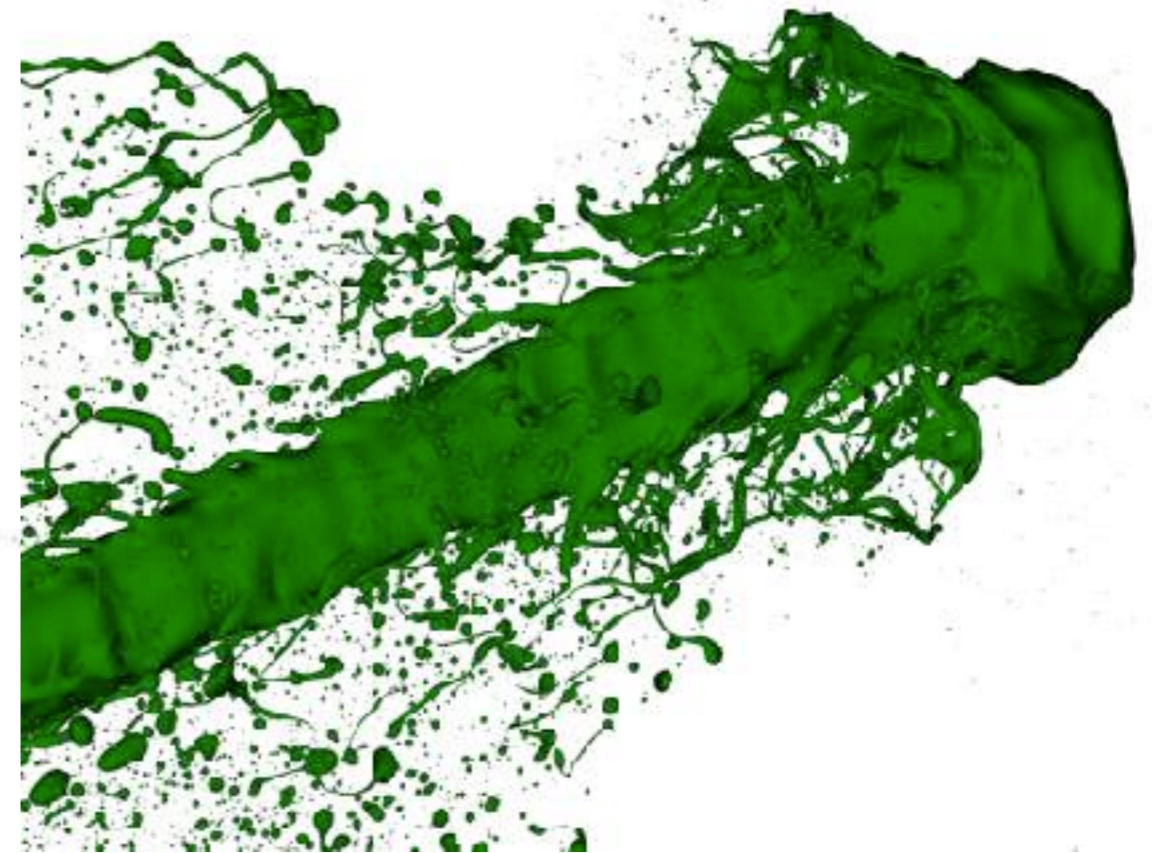
We need better methods to characterize topology!

Summary

- ❖ DNS of atomizing jets are performed for both diesel and biodiesel
- ❖ Sufficient mesh resolution is essential to capturing breakup physics and droplets statistics
- ❖ The most refined mesh yield converged PDF for droplets larger than 3 μm
- ❖ Majority of droplets are formed at mushroom head and hole dynamics play a critical role in sheet breakup
- ❖ The biodiesel jet produces less droplets but of larger size than diesel jet under the same injection conditions

Future Work

- ❖ Topology characterization & statistics
(Ligaments, holes, etc; efficient way to obtain topology & geometry information)
- ❖ More realistic injection condition
(Injection pressure > 1000 bar, $U_{inj} > 200$ m/s)
- ❖ Low fidelity averaging model
(but we need to get a statistically steady state first)
- ❖ Multi-physics
(Droplet evaporation, spray combustion, and more)



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Thank you!